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PREDICTION OF THE SATURN S-II

BASE RADIATION ENVIRONMENT

ENGINEERING REPORT NO. 1469

Prepared for:

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Ву

Sandford A. White John E. Reardon

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1.0 INTRODUCTION

Thermal radiation from rocket exhaust plumes can be a major heating source for the base region of launch vehicles. To provide analytical methods of predicting the radiative flux to this region, the Marshall Space Flight Center has sponsored a series of research studies. This research has led to the development of a method of analysis based on random or statistical band models with a modified Curtiss-Godson approximation for application to inhomogeneous gases (References 1 and 2).

The purpose of this report is to describe the application of the analytical methods to the flux prediction for the S-II stage of the Saturn V launch vehicle. The report concerns itself with three areas of investigation: (1) a method of specifying the gas properties of the exhaust plume for the five-nozzle configuration; (2) a limited investigation of a means of reducing computation time; and (3) the prediction of the radiative flux at selected points in the base region of the S-II stage. The computer program which was developed to numerically evaluate the radiation heat transfer is described in Reference 3.

2.0 EXHAUST PLUME PROPERTIES

In order to specify the exhaust plume properties it is necessary to:

(1) define the engine operating conditions, (2) define the portion of the flow field to be treated, and (3) estimate the gas properties. For the S-II stage the operating conditions are easily defined by the trajectory. But the portion of the flow field to be treated is restricted by computer storage limitations, and the estimation of the gas properties is difficult due to the complex flow geometry.

The S-II stage uses five Rocketdyne J-2 engines arranged as shown in Figure 1. These engines use oxygen and hydrogen as propellants, but the propellant mixture ratio and the nozzle stagnation pressure are varied during the flight. The engines are started on a mixture ratio (oxygen/hydrogen) of 5.0 (by weight), but shortly after starting, the ratio is increased to. 5.5. The 5.5 mixture ratio is maintained for the major portion of the flight (approximately 284 seconds), and then the mixture ratio is reduced to 4.7 for the remainder of the flight (approximately 94 seconds). Maximum radiation from the rocket exhaust occurs at the higher mixture ratio, so the operating conditions chosen for this analysis were the 5.5 mixture ratio and the corresponding nozzle stagnation pressure of 715 psia.

The radiation computer program (Reference 3) requires that the flow field be specified for radial planes in a symmetrical sector about an outboard engine as shown by Figures 1 and 2. The outboard engine was chosen as the center of flow field rather than the center engine, since it simplifies the

preparation of the flow field and requires less computer storage for a given amount of information. The radiation computer program obtains property values in the triangular region c-b-d (Figure 2) about the center engine by using a similarly located point in region a-b-d. This method assumes that plane b-d is a plane of symmetry, and although this is not actually true, it is consistent with the flow field approximation which was used. In the process of the radiation calculation, any point in the exhaust plume is referred to a similar point in the symmetrical sector for which the flow field is defined in order to obtain the gas properties.

Before proceeding with a description of the physical limitations imposed on the flow field by storage limitations in the radiation computer program, it is desirable to consider the limitations and approximations involved with the analytical methods used in estimating the exhaust plume gas properties. At the time the exhaust plume prediction was made, two three-dimensional prediction methods were being developed, but due to the early point in their development cycle there was a lack of confidence that the problem could be successfully solved within the desired time period using these methods. Even if a successful prediction could have been made with one of these methods, it would have been necessary to prepare a computer program or subroutine to interpolate in the output to obtain the proper input form for the radiation program.

Because of the uncertainty and possibility of delay, it was decided to make an approximation using the axisymmetric method of characteristics program described in Reference 4. This program was familiar and had been used successfully many times to prepare input data from axisymmetric plumes for the radiation programs. It allows the use of equillibrium gas properties during expansion and includes a subroutine which will interpolate in the characteristic net to provide gas properties (temperature, pressure, and gas species mole fractions) as a function of radius at specified axial locations.

The axisymmetric program was used to approximate the three-dimensional flow field by making a separate run at each of the η-planes shown in Figure 2. On each run, the plume was expanded from the nozzle exit then turned through an oblique shock into a cylinder with a radius equal to the distance between the engine center line and the impingement plane between engines. Since the pressure ratios at which the S-II engines operate produce detached or normal shocks between plumes, it was necessary to arbitrarily reduce the plume expansion angle until the expanded flow could be turned into the cylinder by an attached oblique shock. To do this, the plume boundary between the nozzle exit and the cylinder was approximated by a cone, and various cone angles were tried until it was determined that a cone angle of 45° was the maximum angle for which the flow could be turned successfully at all cylinder radii.

The resulting flow geometry and isothermal contours are shown in Figure 3 for several representative η-planes, and in Figure 4 for the free-plume boundary which does not intersect an impingement plane. A combination of the predictions is made in Figure 5 to illustrate the variation of temperatures in a cross-section thru the plume.

Although it is not possible to make a quantitative assessment of the accuracy of the flow field approximation, the expected effects are to reduce the temperature in regions near the base and increase the temperature in downstream regions. Effects on the free plume illustrated by Figure 4 are negligible from a radiation standpoint.

The reduced plume impingement angle resulting from the use of the 45° conical transition will not only reduce the physical size of the initial impingement region, but it will also reduce the temperature in the initial impingement. This effect could be quite important for proximate surfaces such as the nozzle exit surfaces, but it would not be as important for more distant surfaces such as the heat shield. An offsetting effect occurs due to the lack of three-dimensional relief as the gas moves downstream. This will cause the gas in the impingement regions to stay at a higher temperature than should actually exist and will result in an increase in plume radiance.

The allowable length of the predicted flow field was limited to 300 inches primarily because of computer storage limitations which will be discussed later. However, while discussing the effects of the flow-field approximation, it is desirable to comment on the flow field aspects affecting the length considerations. The shock positions at various η -planes shown by Figure 6 indicate that at all planes up to η = 35° the shock intercepts the plume center line at less than 300 inches from the nozzle exit. When this occurs in an axisymmetric plume, a Mach disk and shock reflection occurs, and estimates of the flow downstream of this point can be made. But in a three-dimensional

flow field, an axisymmetric type of reflection would not be even a reasonable approximation except on the center engine. This is best illustrated by referring to Figure 5. The shocks converge symmetrically on the centerline of the center engine; but on the outboard engine, the shock approaches the centerline from one side only. By the time the shock reaches the engine centerline, the validity of the approximation is very doubtful, so it was not considered worthwhile to complicate the radiation program geometry by trying to make further estimates of shock shape which would be different for the center and outboard engines. Therefore, the region between the centerline and the position at which the last left running characteristic crossed the 300-inch plane was assumed to be isothermal at the Z = 300 inch, $\eta = 0^{\circ}$ position. The results of this assumption are difficult to illustrate, but the effect may be noted at the 300-inch position in the folow field tabulation presented in the Appendix.

If the flow field had been extended beyond 300 inches, the uncertainty caused by the flow field assumptions would become quite large. Since, as mentioned previously, the basic approximation made should give higher temperatures in the downstream regions, it was considered that this would offset the effects terminating the flow field at 300 inches.

To summarize, the flow field approximation is expected to give lower than desired estimates of temperature in the very beginning of the impingement regions, but it is expected to predict higher temperatures in the downstream portions of the impingement regions. As a result, the radiant heat flux integrated over the entire plume is expected to be a reasonable estimate. Now that

the plume analysis has been reviewed, the description of the radiation program considerations will be completed.

The radiation computer program uses linear interpolation to obtain exhaust plume properties from a table of properties defined as a function of (Z, η, R) as shown by Figure 1. Due to computer storage limitations, the allowable dimensions of this property table were limited to (10, 13, 30). The distribution of the storage between the three dimensions was necessarily somewhat arbitrary but was governed by the following considerations:

- 1) The properties were expected to vary more rapidly in the radial than in the axial direction.
- 2) Although there are no circumferential property variations upstream of the shock caused by the plume impingement, sufficient η -planes need to be provided to try to accurately define the shock shape. This was important since most of the radiation was expected to come from the flow downstream of the impingement shock.

Although the radial positions used throughout the flow field can be varied to best describe the particular flow field conditions, the η and Z positions used must be limited to specific locations to simplify flow field predictions and satisfy requirements of the radiation program. The maximum number of η values used is shown in Figure 2, but some of these could be omitted for convenience where they were not required (i.e., at Z = 0 the plume is axisymmetric so no η dependency exists). These η positions were chosen to provide the best definition of the inner impingement regions which start relatively close to the nozzle exit and expand to significant dimensions as the flow moves

downstream. Similarly, the Z positions were chosen close together initially to define the inner impingement regions (values of Z were 0, 20, 30, 40, 60, 80, 120, 160, 200, and 300 inches). In obtaining a more precise definition of the plume close to the nozzle exit plane, the precision of the downstream definition was sacraficed. However, this is consistent with the probable decrease in accuracy of the flow field approximation downstream of the nozzle.

3.0 COMPUTER PROGRAM

A detailed description of the radiation computer program is given in Reference 3, but it will be described briefly here to provide a background for the results to be presented. In addition to the program outline, descriptions will be presented in this section of the occlusions used in the analysis, and the parametric studies made in selecting integration intervals to reduce computer time.

3.1 PROGRAM DESCRIPTION

The computer program is divided into two subroutines. The first subroutine reads in the flow field listed in Appendix A and prepares a magnetic tape of the gas properties (temperature, pressure, and mole fraction) along each line of sight which passes through the flow field. Lines of sight are specified along radial lines in a spherical coordinate system about a point at which the radiative flux is desired (point of interest). In this coordinate system, S is the distance along the line of sight (or radius vector), θ is the angle between the line of sight and the surface normal, and ϕ is the angle defining the position of the projection of the line of sight in the plane of the point of interest.

The second subroutine takes each line of sight and computes the radiative flux using the summation

$$\stackrel{\circ}{Q}/A = \stackrel{\theta_{f}}{\Sigma} \stackrel{\phi_{f}}{\Sigma} \stackrel{\upsilon_{f}}{\Sigma} \stackrel{s_{f}}{\Sigma} \stackrel{\circ}{\Sigma} - \stackrel{\circ}{B}_{\upsilon} \left[\overline{G}(s,\upsilon) - \overline{G}(s-\Delta s,\upsilon) \right] sin\theta cos\theta \Delta\theta \Delta\phi \Delta\upsilon \quad (1)$$

where B_{υ}° is the black body spectral radiance evaluated at the center of each wave number interval, $\Delta \upsilon$, and \overline{G} is the average transmissivity.

The average transmissivity is computed using a statistical or random band model with a modified Curtiss-Godson approximation to account for the inhomogeneous gas properties. This method is described in Reference 1 as Model 3a, but the line density and absorption coefficients are obtained from Reference 2. Absorption coefficients for water vapor are available over a wavenumber range of 50 to 11000 cm⁻¹ with a spacing of $\Delta v = 25$ cm⁻¹.

3. 2 BLOCKING CIRCLE CONFIGURATION

The occlusion of lines of sight by parts of the S-II stage is provided for in the radiation program by the use of "blocking circles" which can be located to simulate the vehicle structure. The blocking circles are in planes parallel to the X-Y plane, and each is located by the coordinates of the center and the radius. In addition to location, each circle is identified as a disk or a hole. Whenever a line of sight passes through a disk, or outside of a hole, the line of sight is terminated at the plane of the circle.

The occlusions for the S-II stage are described by thirty-six blocking circles as shown in Table 1. Here it is seen that type O specifies a disk and type 1, a hole. Thirty of these blocking circles are used to describe the engine nozzles (six for each nozzle) and are designated as disks. The vehicle skirt is described by one blocking circle which is designated as a hole.

The heat shield is non-circular and as a consequence, is simulated by a configuration of five disks as indicated by the typical quadrant shown in

Figure 7. Here the heat shield is considered to be a disk with a radius of 105 inches, and the peripheral irregularities are simulated by circles of equal area. It is noted that the 105-inch radius blocking circle intersects the five engine nozzles. Since the nozzles are also occluded by disk type blocking circles, no error is introduced by the intersection.

3.3 STUDY OF COMPUTER TIME

In using the exhaust gas radiation computer program for a single line of sight, the computation time is very short. However, when integration over many lines of sight is required, the computation time may be several hours, so a brief evaluation was made of several variables to determine the effect on computation time and accuracy. The variables considered were the geometric step size, the wave number interval, and the minimum absorption coefficient to be considered.

In order to evaluate the effect of these variables, a typical line of sight was chosen for testing. The location of this line of sight is shown by Figure 6. It passes through a plume impingement zone and has temperature and accumulated flux distributions as shown by Figure 8. The minor temperature fluctuations evident along this line of sight are typical of fluctuations caused by the linear interpolation methods used by the radiation computer program for gas properties.

In selecting the geometric limits of S, ϕ , and θ , each limit must be chosen large enough to encompass the entire input flow field, so the problem in selecting the geometry is essentially one of selecting the desired intervals. It is difficult to find a criteria for specifying the optimum angular increments.

 $\Delta \phi$ and $\Delta \theta$, so they were selected as 3 degrees. This provided reasonable resolution and any increment significantly smaller would have produced unreasonable computation times. In contrast, the interval along the line of sight, ΔS , can be varied using a temperature criteria.

The computer program applies a temperature criteria to the increment length along a line of sight by first preparing the properties along a line of sight using a relatively small step size to define the high temperature impingement regions. The properties at each interval are then summed until the temperature change is equal to an input change, ΔT . When this occurs, the properties are averaged, and a term in the summation of Equation 1 is computed. Due to the rapid change of temperature in the plume impingement regions, a ΔS of three inches was chosen for calculating the gas properties. For this basic step size, the effect on computer time, τ , and predicted flux, F, of using temperature increments up to $\Delta T = 200^{\circ}$ R is shown by Figure 9. Because of the significant reduction in computer time with only a minor loss of accuracy, the 200° R temperature increment was selected for all radiation calculations.

An equally effective method of reducing computer time was found in increasing the wave number interval (Δv) used in Equation 1. The radiation computer program requires that the wave number interval be a multiple of the 25 cm⁻¹ interval used in the water vapor absorption coefficient table. For a given problem, the computation time will be approximately inversely proportional to the wave number interval used. This is shown by Figure 10 for wave number intervals of 50 and 100 cm⁻¹. Since a significant saving in

computer time occurred with negligible loss in accuracy using $\Delta v = 100$ cm⁻¹, this interval was selected for the S-II radiation estimates.

Another time-saving variation which was allowed for in the radiation program was a minimum absorption coefficient test. In this option any spectral interval for which the absorption coefficient is below a specified minimum (H_{min}) is neglected. Although this can reduce the computation time, the method in which it was programmed did not allow for maximum effectiveness. The program does not provide any weighting for the absorption coefficient test as a function of the pressure and temperature in the gas. Because of this, significant radiation from a hot, dense region may be neglected due to the absorption coefficient being too low.

The results of the test cases with minimum absorption coefficient ($H_{\rm min}$) values of 10^{-3} and 10^{-2} are presented in Figure 11. Since the time-saving resulting from this option is not great and the results are likely to be of unpredictable accuracy, this option was not used in the S-II radiation prediction.

4.0 RESULTS

Radiation calculations were performed for eight points of interest (POI) in the base region of the S-II stage. These points, shown in Figure 12, represent regions where the maximum radiation heating was anticipated on the heat shield, engine nozzle, thrust cone, and interstage. In addition, the points selected on the heat shield correspond to positions selected for flight measurements with radiation calorimeters.

The radiation calculations were carried out using geometric integration limits which would include the entire exhaust plume approximation described in Section 2. The wave number range used corresponded to the range of available water vapor absorption coefficients, i. e., 50 to 11000 cm⁻¹ (this corresponds to wavelength range of 0.91 to 200 microns).

The results of the radiation predictions are presented in Table 2 with a comparison of previous estimates using a less exact method. Results of the two methods agree surprisingly well, and the heat shield flux is close to the rough estimate of 1.14 watts/cm² (for an engine mixture ratio of 5) which was made before any detailed calculations were carried out (Reference 6). However, the reasonable agreement between the various methods should be considered coincidental.

The computer time (IBM 7094) required initially to generate the flow field was approximately 5 hours and the time required for radiation estimates was a maximum of about 2 hours per point. The radiation calculation time varied greatly in proportion to the number of lines of sight which hit the exhaust

plume and the temperature variations along the line of sight. The time required to perform the flow field interpolation was typically about 10 minutes per point, so the major portion of the run time was required for the detailed radiation calculations.

It should be possible in future estimates to reduce the computer time by deleting a large portion of the short wavelength spectrum (i. e., v = 6000 to 11000 cm^{-1}), but at the time these estimates were made, this method was not used due to lack of sufficient previous experience. In more recent estimates for a line of sight across a J-2 engine plume near the nozzle exit, it was found that 97 percent of the radiant flux from water vapor in the plume lies between wavenumbers of 100 and 6000 cm⁻¹ (wavelengths of 1.67 to 100 microns).

5.0 CONCLUSIONS

This was the first application of the band-model radiation calculation procedure to the prediction of radiant flux from the three-dimensional exhaust plume of a cluster of rocket engines. Although the prediction of the exhaust plume properties involved simplifying approximations, it is believed that similar applications to upper stages are feasible and will provide reasonably accurate estimates. However, a similar application to a plume containing carbon particles or to a plume at low altitude with afterburning would be considerably more difficult and the results much less certain due to the unresolved problems in gas property predictions. It is apparent that the accuracy and feasibility of exhaust plume radiation predictions is now dependent mainly on the availability of satisfactory exhaust plume property prediction methods.

The analytical radiation prediction methods are reasonably well defined at the present time, although it is anticipated that the water vapor band-model parameters will be refined as more experimental data become available.

Further refinements are also planned for future radiation computer programs based on the experience gained in this application. These modifications will be planned to improve input/output flexibility and reduce running time.

6.0 REFERENCES

- 1. "Study of Exhaust Plume Radiation Predictions Interim Progress Report Part II," Contract NAS8-11363, General Dynamics, Convair Division, GD/C-DBE-66-001a, February 1966.
- 2. "Study of Exhaust Plume Radiation Predictions Final Report,"

 Contract NAS8-11363, General Dynamics, Convair Division, GD/C
 DBE-66-017, December 1966.
- 3. Delwadia, M., Reardon, J., and White, S., "A Three-Dimensional Radiation Program for the Saturn S-II Stage," Hayes International Corporation, Engineering Report No. 1470, Contract NAS8-21028, August 1967.
- 4. Prozan, R., "Development of a Method of Characteristics Solution for Supersonic Flow of an Ideal Frozen or Equilibrium Reacting Gas Mixture," Technical Note LMSC/HREL A782536, Lockheed Missile and Space Company, April 1966.
- 5. "Radiation Figures for Inclusion in S-II Final Base Region Thermal Environment," NAA Internal Letter S-II-S&ID 65-658 Addendum I, August 1966.
- 6. Reardon, J. E., "Saturn S-II Stage Base Region Thermal Design Criteria," MSFC Internal Memo M-AERO-A-88-63, August 1963.

TABLE 1. BLOCKING CIRCLE GEOMETRY

X	Y	Z	R	TYPE
0.0000	0.0000	0. 0000	40.0000	0
105.0000	0.0000	0.0000	40.0000	0
-105.0000	0.0000	0.0000	40.0000	0
0.0000	105.0000	0.0000	40.0000	0
0.0000	-105.0000	0.0000	40.0000	0
0.0000	0.0000	-35.7200	32, 2000	0
105.0000	0.0000	-35.7200	32, 2000	0
-105.0000	0,0000	-35.7200	32, 2000	0
0.0000	105.0000	-35, 7200	32.2000	0
0.0000	-105.0000	-35,7200	32, 2000	0
0.0000	0.0000	-40.7200	30.4000	0
105.0000	0.0000	-40.7200	30.4000	0
105.0000	0.0000	-40.7200	30.4000	0
-105.0000	0.0000	-40.7200	30.4000	0
0.0000	105.0000	-40.7200	30.4000	0
0.0000	-105.0000	-40.7200	30.4000	0
0.0000	0.0000	-49.3000	28.1000	0
105.0000	0.0000	-49.3000	28.1000	0
-105.0000	0.0000	-49.3000	28.1000	0
0.0000	105.0000	-49. 3000	28.1000	0
0.0000	-105.0000	-49. 3000	28.1000	0
0.0000	0.0000	-55.9000	28. 2000	0
105.0000	0.0000	-55.9000	28. 2000	0
-105.0000	0.0000	-55.9000	28, 2000	0
0.0000	105.0000	-55.9000	28.2000	.0
0,0000	-105.0000	-55.9000	28. 2000	0
0.0000	0.0000	-62.3000	21.0000	0
105.0000	0.0000	-62.3000	21.0000	0
-105.0000	0,0000	-62.3000	21.0000	0
0.0000	105.0000	-62.3000	21.0000	0
0.0000	-105.0000	-62, 3000	21.0000	0
0.0000	0.0000	-62, 0000	105.0000	' 0
68.6000	68.6000	-62.0000	33.5000	0
-68.6000	68.6000	-62.0000	33.5000	. 0
-68.6000	-68,6000	-62,0000	33,5000	0
68.6000	-68.6000	-62,0000	33,5000	0
0.0000	0.0000	-16.0000	198.0000	1

TABLE 2. POINT OF INTEREST PARAMETERS

POI	x	Y	Z	RADIATIVE WATTS/CM ²	FLUX
	In.	In.	In.	REF. 5	PRESENT WORK
HS-1	52.5	0	-60	0.90	1.11
HS-2	70.711	-70.711	-60	1.18	1.14
NE-1	66.6	0	0	4.20	4.41
NE-2	66.6	0	0	2.04	2.58
TS-1 *	140.0	_140.0	-2 12	0.17	0.15
TS-2 *	124.5	-124.5	-212	0.07	0.05
IS-1	140.0	_140.0	-16	0.73	0.79
IS-2	140.0	-140.0	-16	1.25	1.11

POI Point of Interest

HS Heat Shield

NE Nozzle Exit

TS Thrust Structure

IS Interstage

^{*} The blocking circle corresponding to the interstage skirt was not used for these points.

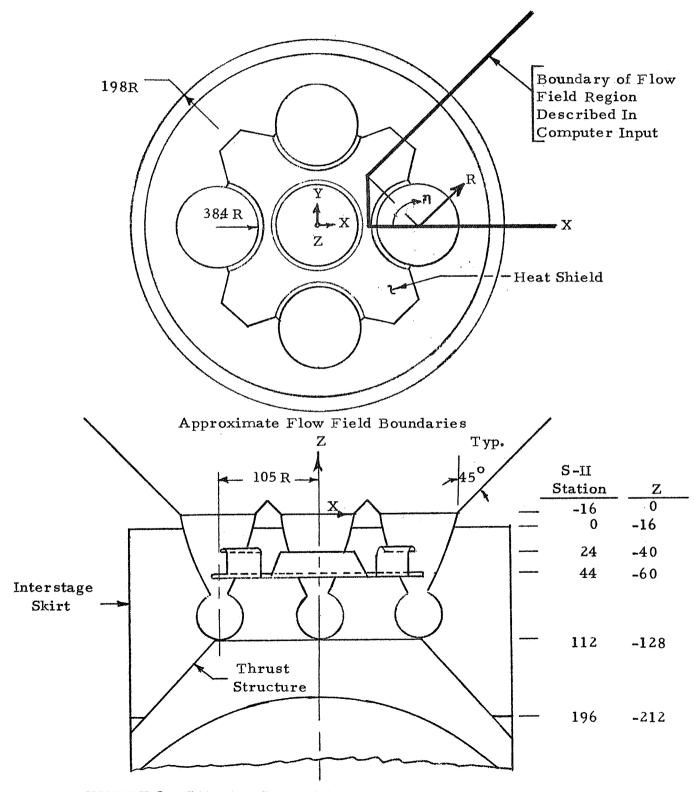


FIGURE 1. SATURN S-II BASE CONFIGURATION AND RADIATION PROGRAM GEOMETRY

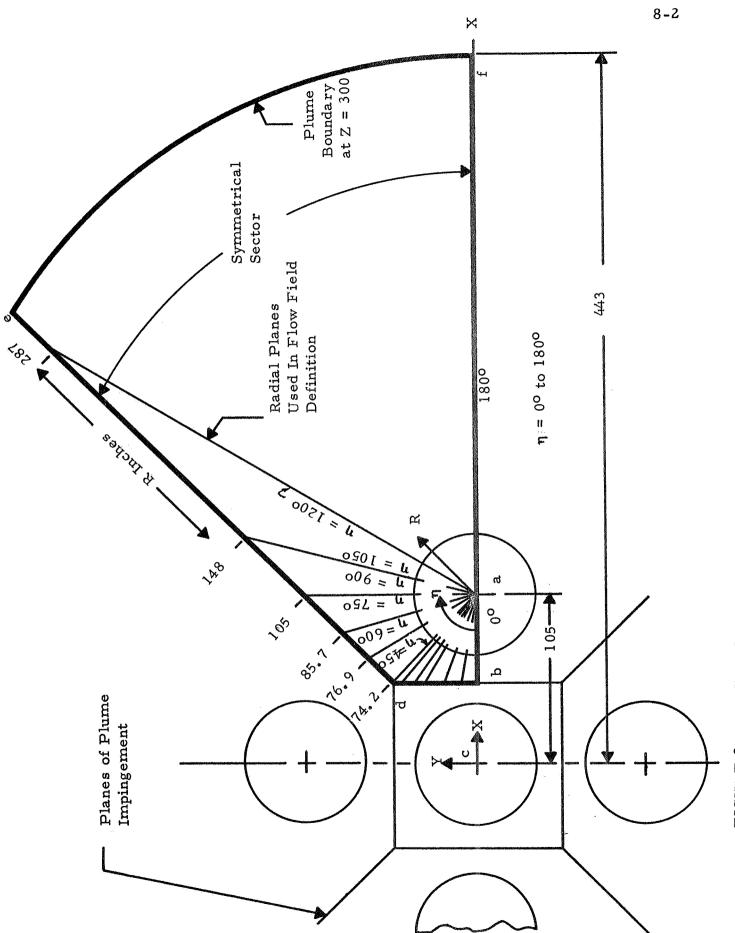


FIGURE 2. FLOW FIELD GEOMETRY FOR S-II RADIATION PREDICTION

- Boundary for Flow Field Approximation
- Isothermal Contours Flow Field Approximation
 All Temperatures in OR

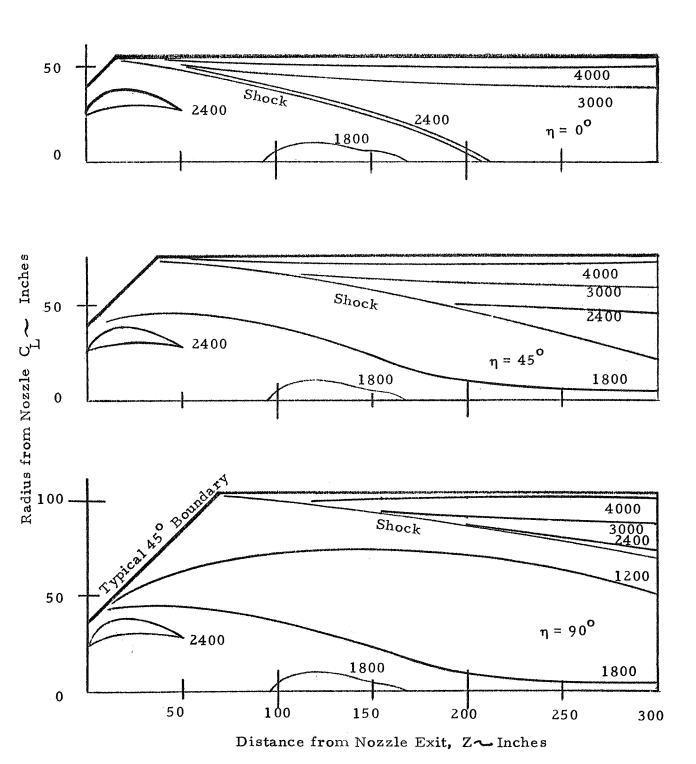


FIGURE 3 . TYPICAL PLUME TEMPERATURES FOR THE S-II FLOW FIELD APPROXIMATION

- Boundary for Flow Field Approximation
- --- Isothermal Contours -- Plume Approximation
- --- Isothermal Contours ~ Free Plume at 240 KFT
- Superimposed Isothermal Contours for Plume Approximation and Free Plume

All Temperatures in ^oR

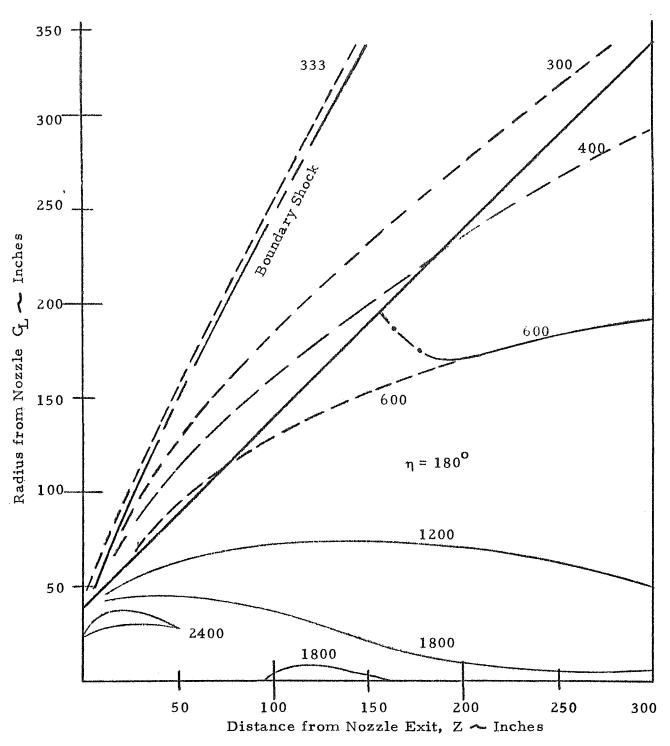


FIGURE 4 . COMPARISON OF FREE PLUME TEMPERATURES
TO THE S-II FLOW FIELD APPROXIMATION

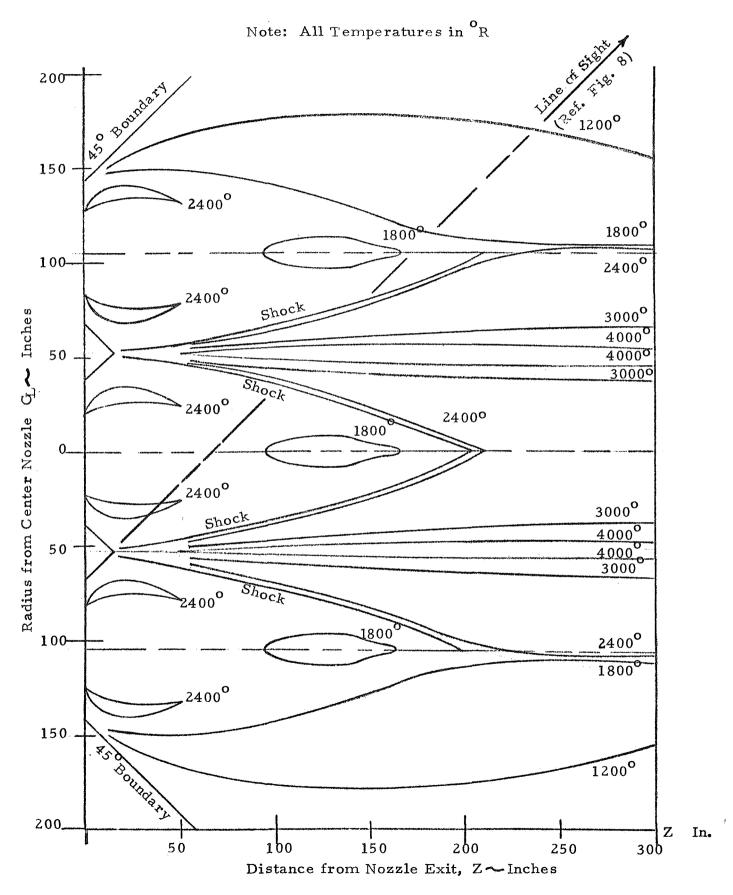


FIGURE 5 . ISOTHERMAL CONTOURS FOR THE X-Z PLANE OF THE S-II FLOW FIELD APPROXIMATION

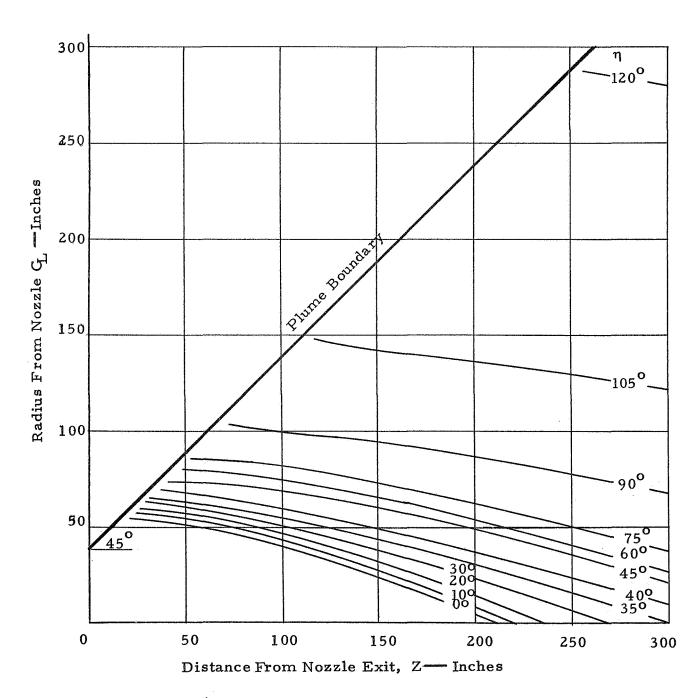


FIGURE 6. SHOCK POSITION FOR THE S-II FLOW FIELD APPROXIMATION

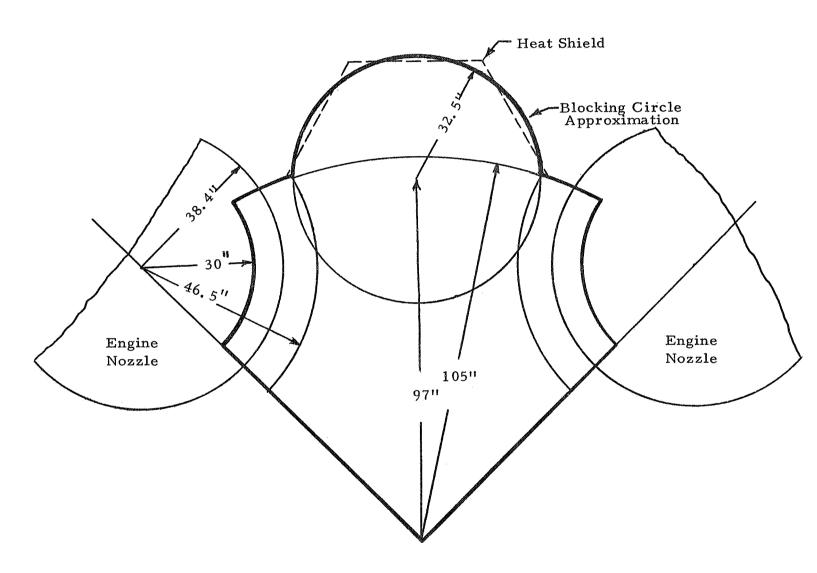


FIGURE 7. HEAT SHIELD BLOCKING CIRCLE APPROXIMATION (SYMMETRICAL QUADRANT)

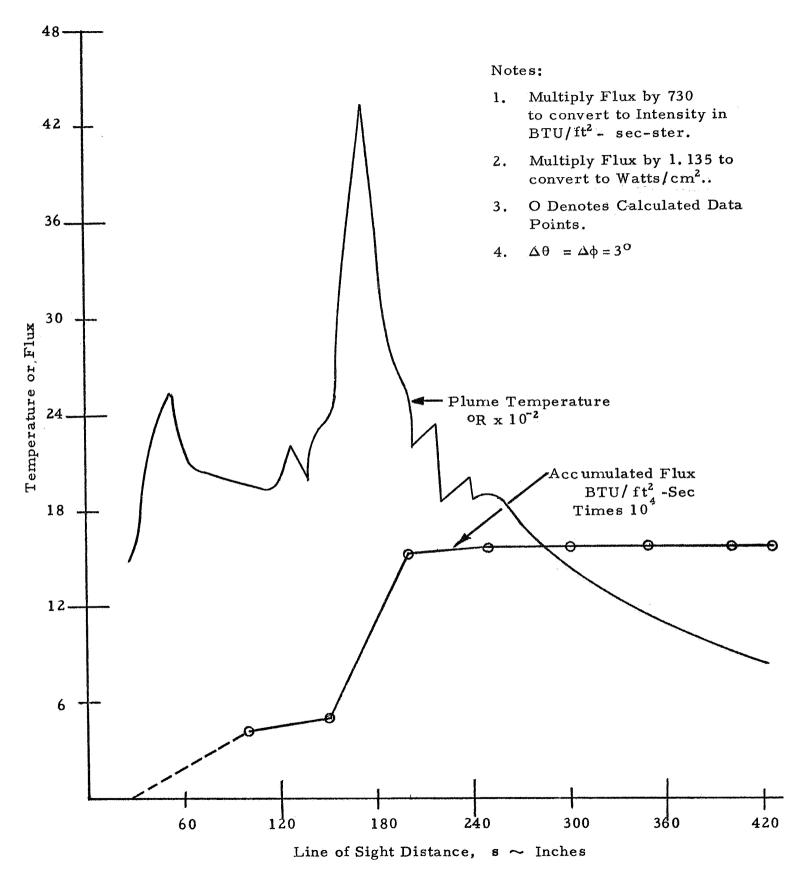


FIGURE 8. COMPARISON OF ACCUMULATED FLUX AND TEMPERATURE PROFILE ALONG A SELECTED LINE OF SIGHT

 τ_r = computer run time based on the reference conditions, $\Delta v = 25$, $\Delta T = 0.0$, and $\Delta s = 3$.

 F_r = computed flux for reference conditions

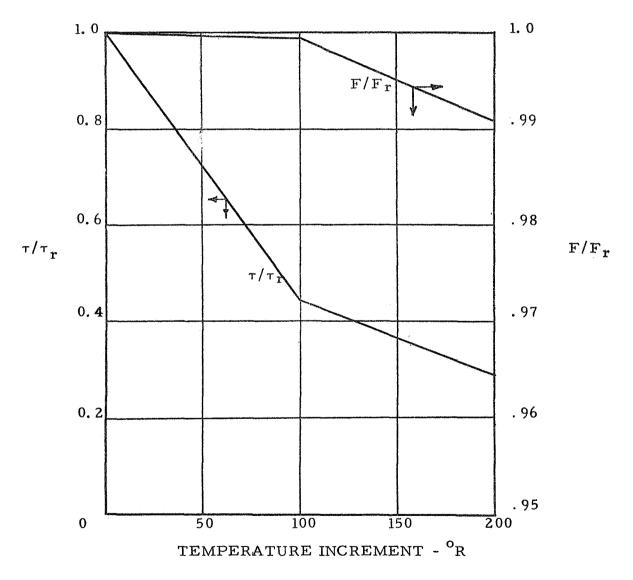


FIGURE 9. EFFECT OF VARYING TEMPERATURE STEP INCREMENT ON COMPUTER RUNNING TIME AND CALCULATION ACCURACY

 τ_r =computer run time based on the reference conditions, H_{min} = 0.000, Δv = 25, ΔT = 0.0, and ΔS = 3 inches. F_r = computed flux for reference conditions

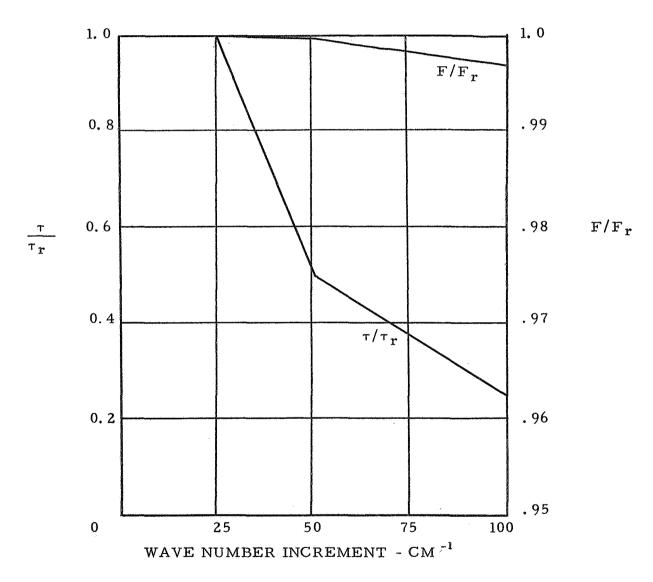


FIGURE 10. EFFECT OF VARYING WAVE NUMBER ON COMPUTER RUNNING TIME AND CALCULATION ACCURACY

 τ_r =computer run time based on the reference conditions, H_{min} = 0.000, Δ_0 = 25, and ΔT = 0.0 F_r =computed flux for reference conditions

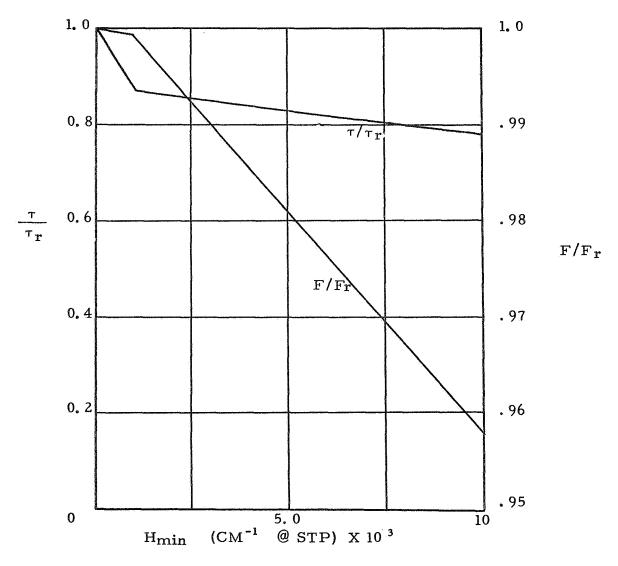


FIGURE 11. EFFECT OF VARYING H_{min} ON COMPUTER RUNNING TIME AND CALCULATION ACCURACY

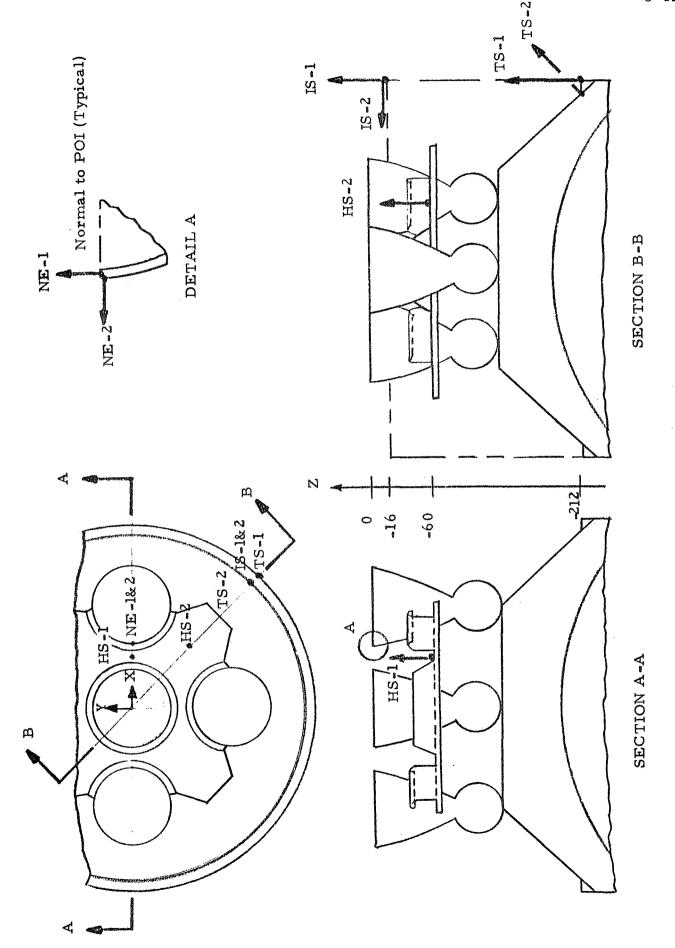


FIGURE 12 LOCATION OF POINTS OF INTEREST

APPENDIX A

S-11 STAGE FLOW FIELD APPROXIMATION. EXPANSION ANGLE AT EXIT IS 45 DEG 02/H2,0/F=5.5,PC=715PSIA

		at the			The same of the sa	
		Z= O.O	NET= 4			
	A first transfer and the second second	NUPS= 28	ETA= O.	o .		
Pot 1 de la company de la comp	R	T	p	F	taning the second se	
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					
	0.0	2343.0	224.0	0.6930		为"自己"。第八次,《新闻》
	10.0	Z343.0	224.0	0.6930		
	12.0	2345.0	225.0	0.6930		
$H_{i} = H_{i}$	13.8	2347.0	226.0	0.6930		
To be a superior of the superi	15.8	2351.0	228.0	~ 0.6930		
	17.5	2360.0	232.0	0.6930		
一型對於自然於於於其他	19.5	2368.0	236.0	0.6930		。
	21.0	2379.0	241.0	0.6930		
	22.5	2391.0	247.0	0.6930		
	24.0	2406.0	255.0	0.6930		
The suffile state of the sufficient of the suffi	25.7	2427.0	266.0	0.6930	<u> </u>	A STATE OF THE STA
	26.9	2449.0	278.0	0.6930		
	28.5	2489.0	301.0	0.6930		
	29.9	2529.0	325.0	0.6930		
	31.0	2570.0	352.0	0.6930		
	32.2	2619.0	388.0	0.6930	the Copley seed	
Jacobilli kali ili aka iri di Alitza ke estra di satati para	33.4	2680.0	434.0	0.6930	The state of the s	
	the second second second second	2716.0	470.0	0.6930		
一门提供 的证明的证明的	34.2	2764.0	514.0	0.6930		生。到一点是阿姆德的
	35.0	2822.0	574.0	0.6930		4 M
	35.9			0.6930		
	36.5	2867.0	623.0	CONTRACTOR OF THE STATE OF THE		
Electrical designation of the second	37.0	2906.0 L	668.0 709.0	0.6930 0.6930	and the state of t	er en de la companya
	37.4	2939.0	756.0	0.6930		
	37.8	2980.0 2997.0	785.0	0.6930	中的位置 医胃透射机	该位500年的为 以外 侧
	38.0 38.2	3018.0	814.0	0.6930		
			822.0	0.6930		
	38.3	3024.0		0.6930		
A STATE OF THE STA	38.4	3034.0	837.0	attechnicus and the contract of the contract o		
上的主义都是不可以	territoria de la companya della companya della companya de la companya della comp	NOPS= 28	ETA= 60.			
	0.0	2343.0	224.0	0.6930		
The state of the s	10.0	2343.0	224.0			
	12.0	2545.0	225 (0)	0.6930		
	13.8	2347.0	225.0	0.6930	and the second second	
	15.8	2351-0	228.0	0.6930	والمتحدد والمحارب والمحادث والمحادث	
White There's	17.5	2360.0	232.0	0.6930		
	19.5	2368.0	236.0	0.6930		
	21.0	2379.0	241.0	0.6930		
	22.5	2391-0	247.0	0.6930		
	24.0	2406+0	255.0	0.6930		
The Control of the Co	25.7	2427.0	266.0	0.6930		
二等。在共和元素的	26.9	2449.0	278.0	0.6930	STATE OF THE STATE	Production and the second
	28.5	2489.0	301.0	. 0.6930		
	29.9	2529.0	325.0	0.6930		
	31.0	2570.0	352.0	0.6930		
	32.2	2619.0	388.0	0.6930	and the second second	
(and the parameter of the later) and the later of the lat	33.4	2680.0	434.0	0.6930		
	Acres 1	7	t in the second			The Court of the C

APPENDIX A (CONTI.)

a sandribera katinga maara sata dhaga ta bib	description of the Market of the Contract of t	ka kan sala idan sana da da ka da da ka sala s	Dingu. maga maskaddanadan industri	an ang an an anakan nakatalan kan kan kan kan nakatalan kan kan kan kan kan kan kan kan kan k
a regional and setting	R	T	P	
	ing a single sin	Short C. A.	47A A	A ZABA
A STATE OF THE STA	34.2 35.0	2716.0 2764.0	470.0 514.0	0.6930 0.6930
	35.9	2822.0	574.0	0.6930
	36.5	2867 . 0	623.0	0.6930
A kalkistan ana kalanda da k	37.0	2906.0	668.0	0.6930
1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	37.4	2939.0	709.0	0.6930
	37.8	2980.0	756.0	0.6930
And the second s	38.0	2997.0	785.0	0.6930
	38.2	9018.0	814.0	ນ.6930
	36.3	3024.0	822.0	0.6930
AND AUGUSTANIA	38.4	3034.0	837.0	0.6930
Maraket Viles	Ne	JPS= 28	ETA=120.0	
建建设设置的	//O.O	2343.0	224.0	0.6930
	10.0	2343.0	224.0	0.6930
	12.0	2345.0	225.0	0.6930
nalkinnaassa vaista saassa seela saakila keel	13.8	2347.0	226.0	.0.6930
素是在基本的主义的	15.8	2351.0	228.0	0.6930 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
作。其代理论是,其实主要	/17.5	2360.0	232.0	0.6930
The state of the s	19.5	2368.0	236.0	0.6930
	21.0	2379.0	241.0	0.6930
	22.5	2391.0	247.0	0.6930
all stances in a mentioner continue the first	24.0	2406.0	255.0	
	25.7	2427.0	266.0	0.6930
	26.9 28.5	2449.0	278.0 301.0	0.6930
	29.9	2529.0	325.0	0.6930
	31.0	2570.0	352.0	0.6930
	32.2	2619.0	388.0	0.6930
A DECREE OF A SECTION OF A SECT	33.4	2680.0	434.0	0.6930
明显混合的振荡主	34.2	2716.0	470.0	0.6930
	35.0	2764.0	514.0	0.6930
	35.9	2822.0	574.0	0.6930
	36.5	2867.0	623.0	0.6930
The Section 1	37.0	2906.0	663.0	0.6930
	37.4	2939.0	709.0	0.6930
	37.8	2580.0	756.0	10.6930
	38.0	2997.0	785.0	0.6930
	38.2	3018.0	814.0	0.6930
	38.3	3024.0	822.0	0.6930
dra facilità a calabra de la c	38.4	3034.0	837 . .	0.6930
	2.5	DPS= 28	ETA=180.0	n 4020
是在BANK TELL AFF	0.0	2343.0	224.0 224.0	0.6930 (7.5%) (8
	12.0	2343.0 2345.0	225.0	0.6930
	13.8	2347.0	226.0	0.6930
	15.8	2351.0	228.0	0.6930
ale a Kining Consideration and a second consideration of	17.5	2360.0	232.0	0.6930
深望,然 性被称。。	19.5	2368.0	236.0	0.6930 ART FREE TO THE STATE OF
· 1988年 1888年 - 1	21.0	2379.0	241.0	0.6930
The Late Control of the Control of t	22.5	2391.0	247.0	0.6930
	24.0	2406.0	255.0	0.6930
agenta agenta de la companya de la c	25.7	2427.0	260.0	0.6930
AMERICAN AND AMERICAN PROPERTY AMERICAN PROPERTY AND AMERICAN PROPERTY AMERICAN PR	· · · · · · · · · · · · · · · · · · ·	1904 - A. 1904 - A. Tananananananananananananananananananan	namente en 1900 partemos : en 1900 de la partemos d La partemos de la pa	

a de la companya de					
. 1888 (1886) danel da Madalla (1881) da Cara	8	T	p	F	
1224 South and Approximate Control (1888) The Control of Control o	26.9	2449.0	278.0	0.6930	
	28.5	, 2489.0	301.0	0.6930	
	29.9	2529.0	325.0	0.6930,	and the state of t
to destruction to the second second second	31.0	Decougae (CONTRACTOR) and CONTRACTOR CONTRAC	/352.Q	0.6930	an an in the state of the state
	32.2 33.4	2619.0 2680.0	388.0 434.0	0.6930 0.6930	
	34.2	2716.0	470.0	0.6930	
	35.0	2764.0	514.0	0.6930	
	35.9	2822.0	574.0	0.6930	
j.	36.5	2867.0	623.40	// 0.6930	
	37.0	2906.0	668.0	0.6930	
国教教 医氯化双酚	37.4	2939.0	709.0	0.6930	
######################################	37.8	2980.0	756.0	0.6930	
	38.0	* 2997.0	785.0	V.6930	
	38.2	3018.0	814.0	0.6930	
dia prindica di manda	38.3	3024.0	Jul 822.0	5.6930	diadasa dikabanga pada basa watawa ninga pada ata da da da basa na m
	38∘4	3034.0 Z= 20.0	837.0 NET= 7	0.6930	
		NOPS= 29		。O	
	U.0	2343.0	224.0	0.6930	
	2.9	2328.0	217.0	0.6930	
	3.7	2317.0	212.0	0.6930	
NO NOTICE AND DESCRIPTION OF THE PROPERTY OF T	5.0	2296.0	203.0	0.6930	
	9.1	2232.0	177.0	0.6930	
	11.1	2206.0	167.0	0.6930	
	13.5	2184.0	159.0	U.6930	
	15.9	2182.0	159.0	0.6930	
er allah persikentah menada mahingga persika.	18.3	2187.0	160.0	0.6930	entre distribution describing à l'établisse de l'établisse de partie de la partie de la figure de la figure de
	20.4	2197.0 2217.0	164.0 171.0	0.6930 0.6930	1. 5. 1. 4. 数 1. 数 1. 数 1. 数 1. 数 1. 数 1. 数
	24.9	2244.0	182.0	0.6930	그 돌아왔다. 생활한 사람은 경험 경험이 모임하다
	27.2	2295.0	203.0	0,6930	
	28.9	2350.0	228.0	0.6930	
•	30.6	2428.0	266.0	0.6930	
	32.1	2547.0	336.0	0.6930	
	33.7	A contract of the contract of	522.0	0.6930	인민 아들은 왔었다. 본 등은 사용적 시간 등
	34.8	2681.0	439.0	0.6930	
e de la companya de La companya de la co	36.5	2538.0	330.0	0.6930	
	38.2	2377.0	240.0	0.6930	
	39.7 41.7	2229.0 2039.0	176.0 114.0	0.6930 0.6930	<u> Baran Santan Maria Masaktera (j. 1864)</u>
	44.1	1804.0	65.0	0.6930	
	46.1	1622.0	40.0	0.6930	
	48.6	1404.0	21.0	0.6930	
	51.3	1200.0	11.0	0.6930	
	51.5	4110.0	288.0	0.6830	
	51.9	4420.0	280.0	0.6590	
	52,5	4495.0	280.0	0.6490	**
		NOPS= 29	ETA= 10		
	0.0	2343.0	224.0	0.6930	
	2.9 3.7	2328.0 2317.0	217.0 212.0	0.6930 0.6930	
	2e l 5 . 0	2296 ₃ 0	203.0	0.6930	
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		APPENUIX A	en al			
	R 9.1	T 2232.0	P 177.0	F 0.6930		
	11.0 13.5	2206.0 2184.0	167.0 159.0	0.6930 0.6930		
	15.9 18.3	2182.0 2187.0	159.0 160.0	0.6930 0.6930	medas iksipiotoriumiperijorius iksipi	k saas saang paramaan in t
	20.4	2197.0 2217.0	164.0 171.0	0.6930 0.6930 0.6930		
	24.9 27.2 28.9	2244.0 2295.0 2350.0	182.0 203.0 228.0	0.6930 0.6930		
gallansian engagan susan inspecient and an analysis and an ana	30.6 32.1	2428.0 2547.0	266.0 336.0	0.6930 0.6930		
	33.7	2772.0 2681.0	522.0 439.0	0.6930 0.6930 0.6930		
	36.5 38.2 39.7	2538.0 2377.0 2229.0	330.0 240.0 176.0	0.6930 0.6930	in the second se	
	41.7	2039.0 1804.0	114.0 65.0	0.6930 0.6930		
	46.1 48.6	1622.0 1404.0 1125.0	40.0 21.0	0.6930 0.6930 0.6930		
	52.3 52.4 52.5	1121.0 4243.0	8.3 8.3 269.0	0.6930 0.6930		
	53.3 Ni	4476.0 JPS= 30	264.0 ETA= 20.0	0.6510		
	0.0 2.9 3.7	2343.0 2328.0 2317.0	224.0 217.0 212.0	0.6930 0.6930 0.6930		Kanasia sa ji landara ka 191
	5.0 9.1	2296.0	203.0	0.6930 0.6930		
	11.1 13.5	2206.0 2184.0	167.0 159.0	0.6930 0.6930		
	15.9 18.3 20.4	2182.0 2187.0 2197.0	159.0 160.0 164.0	0.6930 0.6930 0.6930		
	22.9 24.9	2217.0 2244.0	171.0 182.0	0.6930 0.6930		
	27.2 28.9 30.6	2295.0 2350.0 2428.0	203.0 228.0 266.0	0.6930 0.6930 0.6930		
	32.1 33.7	2547.0 2772.0	336.0 522.0	0.6930 0.6930		
	34.9 36.5	2681.0 2538.0	439.0 330.0	0.6930 0.6930		
	38.2 39.7 41.7	2377.0 2229.0 2039.0	240.0 180.0 114.0	0.6930 0.6930 0.6930		
	44.1 46.1	1804.0 1622.0	65.0 40.0	0.6930 0.6930		
	48.6	1404.0	21.0	0.6930		
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		APPENDIX A	(CONTI.)			di. s
eli, e de escolitorio escala (Corolladore de La Corolladore de La		grande Landing of State and Maria (1. 11 State 1921)	Marine and the first of the second	<u></u>	ne aleman de la companya de la comp	<u>Markaret best best best also a como</u>
	R		P	•		
1.	52.3 55.3	1122.0 // L082.0	8.3 7.1	0.6930 0.6930		
	55.4 55.5	4276.0 4469.0	253.0 250.0	0.6720 0.6500	general State of the Mark	
	55.9	4467.0	250.0	0.6500	The second secon	
	0.0	NOPS= 29 2343.0	ETA= 30.0 224.0	0.6930		to the substitute and case the substitute of the
	2.9 3.7	2328.0 2317.3	217.0 212.0	0.6930 0.6930		
<u>Santan Balanda</u>	5.0	2296.0	203.0	0.6930	aringmanically and their knows were the	<u> </u>
	9.1 11.1	2232.0 2206.0	177.0 167.0	0.6930 0.6930		
	13.5	2184.0	159.0 159.0	0.6930		
	15.9 18.3	2182.0 2187.0	190.0	0.6930	Parada di Parada di Basala Parada	
<u> </u>	20.4 22.9	2197.0 2217.0	164.0 171.0	0.6930 0.6930		<u> </u>
	24.9	2244.0	182.0	0.6930		
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	30.6	2428.0	266.0 336.0	0.6930 0.6930		
The first process of the sales are a second	32.1 33.7	2547.0 2772.0	522.0	0.6930		Militaria di Ambilia di Marini de Santo di Marini di Marini di Marini di Marini di Marini di Marini di Marini Militaria di Marini
	34.9	2681.0 2538.0	439.0 330.0	0.6930 0.6930		
	38.2	2377.0	240.0	0.6930		
	39.7 41.7	2224.0 2039.0	180.0 114.0	0.6930 0.6930		Hara allegar sala
	44.1	1804.0	65.0 40.0	0.6930 0.6930	3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	46.1	1622.0 1404.0	21.0	0.6930	3 Marie - 10 Marie - 1	
	52.3 55.6	1122.0 1081.0	8.3 7.1	0.6930 0.6930	1 Grand State of State	
	58.3	1071.0	6.9	0.6930		Marie Caracan and an article and an article and the second and the
	58.4	1071.0 NOPS= 29	6.9 ETA= 60.	0.6930 0		
	0.0	2343 _* 0. 2328 _* 0	224.0 217.0	0.6930 0.6930		
	2.9 3.7	2317.0	212.0	0.6930		
	5.0 9.1	2296.0 2232.0	203.0 177.0	0.6930 0.6930	and the same of th	
	11.1	2206.0	167.0	0.6930		ja se Projekt
	13.5	2184.0 2182.0	159.0 159.0	0.6930 0.6930		
List of the state	18.3	2187.0	160.0 164.0	0.6930 0.6930		
	20.4 22.9	2197.0 2217.0	171.0	0,6930		ogilistististististististististististististi
	24.9	2244.0 2295.0	182.0 203.0	0.6930 0.6930	. 5	
	28.9	2350.0	228.0	0.6930		
	30.6 32.1	2428.0 2547.0	266.0 336.0	0.6930 0.6930		<u> Der Brander i grand Blander and de la companya de</u>
A SEAL OUR DECEMBER OF THE PROPERTY AND THE SEAL OF THE PROPERTY AND THE P	A STREET, SANGER STREET, SANGER	- The second	{		,	

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The said said said.	4.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1	1 200
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	20 2	2772 0	. 50 0 6	0 (030	
	33.7	2772.0 2681.0	522.0 439.0	0.6930 0.6930	
	36.5	2538.0	330.0	0.6930	
on alternative in the first of the state of	38.2	2377.0	240.0	0.6930	and the second of the second o
	39.7	2224.0	180.0	0.6930	
	41.7	2039.0	114.0 65.0	0.6930 0.6930	
	46.1	1622.0	40.0	0.6930	
	48.6	1404.0	21.0	0.6930	
	152.3	1122.0	8.3	0.6930 0.6930	
	55.6 58.3	1081.0 1071.0	7.1 6.9	0.6930	
	58.4	1071.0	6.9	0.6930	
		NOPS= 29	ETA=120.		
	0.0	2343.0	224.0	0.6930	
	2-9 3.7	2328.0 2317.0	217.0 212.0	0.6930 0.6930	ikani kaping Canada in Kaping dia kang kang 1918 di 1919 at Panjah Panjah Panjah Panjah
中国人员的 1777 ·	5.0	2296.0	203.0	0.6930	
	9.1	2232.0	177.0	0.6930	
	11.1	2206.0	167.0	0.6930 0.6930	
	13.5 15.9	2184.0 2182.0	159.0 159.0	0.6930	
	18.3	2187.0	160.0	0.6930	
	20.4	2197.0	164.0	0.6930	
	22.9 24.9	2217.0 2244.0	171.0 182.0	0.6930 0.6930	
	27.2	2295.0	203.0	0.6930	
	28.9	2350.0	228.0	0.6930	
	30.6	2428.0	266.0	0.6930	
	32.1 33.7	2547.0 2772.0	336.0 522.0	0.6930 0.6930	
	34.9	2681.0	435.0	0.6930	
	36.5	2538.0	330.0	0.6930	
	38.2	2377.0	240.0	0.6930	an a
	39.7 41.7	2224.0 2039.0	180.0 114.0	0.6930 0.6930	
	44.1	1804.0	65.0	0.6930	
	46.1	1622.0	40.0	0.6930	
	48.6 52.3	1404.0 1122.0	21.0 8.3	0.6930 0.6930	
	55.6	1081.0	7.1	0.6930	
	58.3	1071.0	6.9	0.6930	
	58.4	1071.0	6.9	0.6930	
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	2.9	2328.0	217.0	0.6930	
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	5.0	2296.0	203.0	0.6930	
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	13.5	2184.0	159.0	0.6930	
	15.9	2182.0	159.0	0.6930	
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$^{\circ}$	0.0	753	135	S	223	12.0	341	7.6	200	300	8,77	52.3	CS-2	777	7	9972			20	23.00	67.83	44	132	77
2	٠.	ж.			m	477	•	2 F	100	* 3	60.0	61.4	70				0.5	7.	А.	180 a		113	7.0	(22
iii		6.3		<i>.</i>	*			1	1	2100	43	12.0	ш.	4. 0		4			n	C 1.		A 160		28

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		APPENDIX	A (CONTIA)		
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	1% (. ≇	•	•	
	100	0107 0	1/0 0	0 (020	그 그 그는 그는 지수 하지만 설팅하셨다.
	18.3	2187.0	160.0	0.6930	
	20.4	2197.0	164.0	0.6930	
	22.9	2217.0	171.0	0.6930	
	24.9	2244.0	182.0	0.6930	
and the contract and the contract of the contr	27.2	2295.0	203.0	0.6930	miliodellusiaminemineminemineminemineminemineminemine
	28.9	2350.0	228.0	0.6930	입니어 아이 그 살아왔는데 그는 이 이름 때문을 다녔다.
	and the second second				그리기 그 얼마나 아이들은 없게 되어야할?
	30.6	2428.0	266.0	0.6930	
	32.1	2547.0	336.0	0.6930	
	33.7	2772.0	522.0	0.6930	
4	34.9	2681.0	439.0	0.6930	
TO SECURITION OF	36.5	2538.0	330.0	0.6930	THE PERSON NAME OF THE PERSON NA
그렇게 다시 되었다.	38.2	2377.0	240.0	0.6930	
	39.7	2224.0	180.0	0.6930	
	41.7	2039.0	114.0	0.6930	
	44.1	1804.0	65.0	0.6930	
	46.1	1022.0	40.0	0.6930	
ACCOUNT OF THE PROPERTY OF THE	48.6	1404.0	21.0	0.6930	THE CONTRACT OF THE CONTRACT O
	52.3	1122.0	8.3	0.6930	
그렇게 되었다. 그렇게 뭐	55.6	1081.0	7.1	0.6930	
	58.3	1071.0	o . 9	0.6930	
	58.4	1071.0	6.9	0.6930	
		Z= 30.0	NET= 11		
		NOPS= 28	ETA= 0.0	0	
	0.0	2304.0	207.0	0.6930	
	1.6	2294.0	202.0	0.6930	
	3.5	2264.0	190.0	0.6930	
				Contracting the contracting of t	
	5.5	2234.0	178.0	0.6930	
and the second second second second second	7.7	2205.0	167.0	0.6930	
	9.8	2178.0	157.0	0.6930	State of the state
	12.0	2155.0	149.0	0.6930	
	13.9	2135.0	143.0	0.6930	
	16.5	2120.0	138.0	0.6930	
	19.1	2125.0	139.0	0.6930	
	21.7	2141.0	145.0	0.6930	
a 1918 julia (kandalah dalah kada (kada da kada da kada da ka	**********************	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	**************************************		and the state of the
그림 닭 맛이 걸 먹다 하	23.9	2168.0	154.0	0.6930	
二次法學問籍(4) (2) 转录计	26.5	2225.0	174.0	0.6930	
	28.5	2307.0	208.0	0.6930	
	30.7	2642.0	407.0	0.6930	
	32.2	2613.0	383.0	0.6930	
	33.7		327.0	0.6930	
	35.4	2434.0	270.0	U.6930	
	37.5	2308.0	208.0	0.6930	
Street P. Control of the Control of	39.1	2207.0	168.0	0.6930	
	41.6	2054.0	118.J	0.6930	
	44.1	1894.0	81.0	0.6930	
	46.4	1748.0	56.0	0.6930	
ar pagalitiks nikobandaa ameentaning arabahan beer kan	49.5	1567.0	34.0	0.6930	
	50.3	1509.0	27.0	. 0.6930	
	50.4	1500.0	27.0	0.6930	
	50.6	3690.0	395.0	0.6900	
	52.5	4670.0	431.0	0.6350	
Carlo da sala da la carlo de la carlo d		NOPS= 28	ETA= 10.0	<u>)</u>	
	0.0	2304.0	207.0	0.6930	
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A State of the sta	on a series	La de la companya de			A Company of the Comp
A STANTON TO A CONTROL OF THE STANTON OF THE STANTO	R	T	P	F	
A STATE OF THE PROPERTY OF THE	1.6	2294.0	202.0	0.6930	
	3.5 5.5	2264 . 0 2234 . 0	190.0 173.0	0.6930 % 0.6930	
	7.7	2205.0	167.0	0.6930	
(come, in a single addressed of the Continue Come (in the Continue	9.8	2178.0	157.J	0.6930	and the state of t
	12.0	2155.0	149.0	0.6930	
•	13.9	2135.0	143.0	0.6930	
	16.5	2120.0	138.0	0.6930	and the second second second
	19.1	2125.0	139.0	0.6930	
and the second s	21.7. 23.9	2141.0 2168.0	145.0 154.0	0.6930 0.6930	
	25.5	2225.0	174.0	0.6930	
	28.5	2307.0	208.0	0.6930	
	30.7	2642.0	407.0	0.6930	
	32.2	2013.0	383.0	0.6930	
	7. و د د .	2532.0	327.0	0.6930	<u>inadio della parte di di propinti di di di di propinti di di</u>
	35.4	2434.0	270.0	0.6930	一点 网络人名英克克克塞尔
	37.5 39.1	2308.0 220 7. 0	208.0	0.6930 0.6930	그는 이번에 현대를 원래 제 없는
	41.6	2054.0	168.0 118.0	0.6930	
	44.1	1894.0	81.0	0.6930	
	46.4	1748.0	55.0	0.6930	
Provide the Contraction of the C	49.5	1565.0	34.0	0.6930	
	51.3	1475.0	25.0	0.6930	
	51.4	3750.0	376.0	0.6890	
	52.4 53.3	4284.0 4647.0	391.0 404.0	0.6720 0.6370	
	ر ه د د	NOPS= 29	ETA= 20.		
	0.0	2304.0	207.0	0.6930	
	1.6	2294.0	202.0	0.6930	
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	13.9	2135.0	143.0	0.6930	
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	46.4	1748.0	56.0	0.6930	
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(27.50. Lond 11.56.11 Security (2. 150.150.12.11 Security)	R	T	P	F	kat amangistanadi santik intakka kurda (biraka penenena kindilah istahan intakka biraka biraka bawa
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	49.5 53.4	1565.0 1346.0	34.0 18.0	0.6930 0.6930	
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	54.1	4000.0	311.0	0.6870	i geri sahija sahihata bibili siliri (12 ba Abil abbaha debelah
	55.3 55.9	4434.0 4564.0	320.0 319.0	0.6600 0.6430	
		NOPS= 30	ETA= 30.0		
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	7.7	2205.0	167.0	0.6930	
	9.8	2178.0 ***/2155.0	157.0 149.0	0.6930 0.6930	
	13.9	2135.0	134.0	D.6930	
	16.5	2120.0	138.0	0.6930	<u> </u>
	19.1 21.7	2125.0 2141.0	139.0 145.0	0.6930 0.6930	
	23.9	2141.0	154.0	0.6930	
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	28.5	2307.0	208.0	0.6930	
dijus kojaji kus kantunga, ila kansah sa 2002, ila kantania	30.7 32.2	2642.0 2613.0	407.0 383.0	0.6930 0.6930	D 18 M o Camar Diago marabalta produce admillura dos comerciones
	33.7	2532.0	327.0	0.6930	
	35.4	2434.0	270.0	0.6930	
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	41.6	2054.0	118.0	0.6930	
340	44.1	1894.0	81.0	0.6930	
	46.4 49.5	1748 _* 0 1565 _* 0	56.0 34.0	0.6930 0.6930	
	53.4	1344.0	18.0	0.6930	
	56.6	1181.0	10.0	0.6930	
	59.0 59.1	1089.0 4119.0	6.7 283.0	0.6930 0.6790	
	59.9	4433.0	214.0	0.6520	
11 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	60.7	4429.0	214.0	0.6530	
	0.0	NUPS= 30 2304.0	ETA= 35. 207.0	0	
	1.0	2294.0	202.0	0.6930	and the state of t
***	3.5	2264.0	190.0	0.6930	BEATH CHANGE THE STREET CONTRACT CHANGE THE STREET CHANGE TO THE CONTRACT CHANGE THE C
	5.5 7.7	2234 _* 0 2205 _* 0	178.0 167.0	0.6930 0.6930	in the second se
	9.8	2178.0	157.0	0.6930	
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	16.5	2120.0 2125.0	138.0 139.0	0.6930	
	21.7	2141.0	145.0	0.6930	
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Car Land Obel Charles (Call Carlos Charles Cha	R	T	Р	F	
	30.7	2642.0	407.0	0.6930	
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	41.6	2054.0	118.0	0.6930	
	44.1 46.4	1894.0 1748.0	81.0 50.0	0.6930 0.6930	
antena, de esta en estado de discoso	49.5	1555.0	34.0	0.6930	<u>Community of the last of the </u>
	53.4 56.6	1344.0 1181.0	18.0 10.0	0.6930 0.6930	
	60.7	1627.0	5.8 5.6	0.6930 0.6930	
	63.3 63.4	1001.0 4286.0	210.6	0.6740	
	64.1	/4432.0 NOPS= 30	207.6 ETA= 40.	0.6510	
	0.0	2304.0	207.0	0.6930	·*
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a nama kan kan ang kanalang kan ang kanala	7.7 9.8	2205.0 2178.0	167.0 157.0	0.6930 0.6930	
v i	12.0	2155.0	149.0	0.6930	.
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ik Tanan kanan ka	26.5 28.5	2225.0 230 7. 0	174.0 208.0	0.6930 0.6930	
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	35.4	2434.0	270.0	0.6930	
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	44.1 46.4	1894.0 1748.0	81.0 56.0	0.6930 0.6930	
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	56.6	1181.0	10.0	0.6930	
September 1981	60.7 65.6	1027.0 1011.0	5.8 5.4	0.6930 0.6930	
	67.3	1003.0	5.3	0.6930	
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	0.0	2304.0	207.0	0.6930	
	1.6 3.5	2294.0 2264.0	202.0 190.0	0.6930 0.6930	
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1		. '			in the state of th

44.8	 about More of				32.24		. 2	1		w.
- A	 PEI		1 1	- C. 34	200	્⊈ે (* N		1000	ř.
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is mil estat un enticonadore dos entre y la suctuanidad representa	R	T	P	F	MOLE WITH THE PROPERTY OF THE CONTROL OF THE SHARE SHARE SHARE AND SHARE AND THE SHARE SHA
	7.7	2205.0	167.0	0.6930	
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	19.1	2125.0	138.0	0.6930	
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	28.5	2307.40	208.0	0,6930	
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i lega ki astisi da hikiki libasi da k	41.6	2207.0 2054.0	168.0 118.0	0.6930	
of my surprise	44.1	1894.0	81.0	0.6930	
	46.4	1748.0	56.0	0.6930 0.6930	
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Terretarion de la constante de	7.7	2205.0	167.0	0.6930	
	9.8 12.0	2178.0 2155.0	157.0 149.0	0.6930 0.6930	is a superior and property of the superior of
	13.9	2135.0	134.0	U.6930	
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	32.2	2613.0	383.0	0.6930	
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	35.4 37.5	2434.0 2308.0	270.0 208.0	0.6930 0.6930	
	39.1	2207.0	168.0	0.6930	
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	44.1	1894.0 1748.0	81.0 56.0	. 0.6930 0.6930	
	49.5	1565.0	34.0	0.6930	
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<u> </u>					

K	Tank Alak Alaman a sa s	alie da per per de la compansión de properties de la compansión de la compansión de la compansión de la compan La compansión de la compa	r og skrivet for state of the second state of the second s	and the second second of the second
56 d	can a conservation of the form of the property	10.0	0.6930	Process of the control of the contro
,,,60.		5.8	0.6930	
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9,	.8 2178,0	157.0	0.6930	/
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16.	は、1988年に対象が1.5分割が発えていた。たいとして、これません。	138.0	0.6930	
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21/20/20/20/20/20/20/20/20/20/20/20/20/20/	Marie Anna American Sold of Alles & Assessment of the Assessment o		0.6930 0.6930	tirin jan Sibori nibara maanik seel kaini aftiridi kunnest (in alterite illinbari 1888).
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\mathcal{A}_{44}^{1}	· " 打造 2016 我没有 我就是这个一定的证据。" " 对 2016 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16		0.6930 0.6930	
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49.	ar berte kanner værene de kolonieren.	34.0	0.6930	a tanahir mendalah dalam sarah kerebah dan dia dan dia dan kerebah dia dan dalam dan dan dan dan dan dan dan d
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60		Party and the second of the second of the second of the second	0.6930	and the second of the second o
65		5.4	0.6930	and the second
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- 4		APPENDIX	A (CONTI.)		
			Edit China de la casa	e decidloloxicom o successiva de cor e considerabilità con es	Nakatin ilitaari maalila apka sa aksastiika sa shaktiin si ka sa ka sa ka sa ka sa ka kishiishii shaktiishii
1 2 4	R	T	Р	F	H (1986)
	35.4	2434.0	270.0	0.6930	
	37.5 39.1	2308:0 2207:0	208.0 168.0	0.6930 0.6930	
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	46.4	1748.0	56.0	0.6930	
	49.5 53.4	1565.0 1344.0	34.0 19.0	0.6930 0.6930	
	56.4	1181.0	10.0	, °0.6930∜	and the second property of the second second
	60.7 65.6	1027.0 1011.0	5.4	0.6930 0.6930	
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	0.0	2304.0	207.0	/. U.6930 ///	
	1.6 3.5	2294.0 2264.0	202.0 190.0	0.6930 0.6930	
	5.5	2234.0	178.0	0.6930	CHIESTANIAN MATERIALI MENTERIA DE ANGRE PARTON MET PARTON PROPERTA EN METALE MESTANIAN BENEFA PARTON. METALEMAN MATERIALI METALEMAN PROPERTA METALEMAN METALEMAN PARTON PROPERTA METALEMAN PROPERTA METALEMAN PROPER
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a de la compania de La compania de la co	16.5	2120.0	138.0	0.6930	
	19.1 21.7	2125.0 2141.0	139.0 145.0	0.6930 0.6930	
	23.9	2168.0	154.0	0.6930	Takan bar sementa cama ke takan pan kun da sakan dalah dan kanan kun ke tahun takan da bara bara bar bar bar b
Paris Property (1994)	26.5 28.5	2225.0 2307.0	174.0 208.0	0.6930 0.6930	
	30.7 32.2	2642.0 2613.0	4 07. 0 383.0	0.6930 0.6930	
	33.7	2532.0	327.0	0.6930	
	35.4 37.5	2434.0 2308.0	270.0 208.0	0.6930 0.6930	
	39.1	2207.0 2054.0	168.0 115.0	0.6930 0.6930	
go anidi diganamendika mpuliga gairje	41.6 44.1	1894.0	81.0	0.6930	
	46.4 49.5	1748.0 1565.0	56.0 34.0	0.6930 0.6930	·
	53.4	1344.0	18.0	0.6930	
	56.6 60.7	1181.0 1027.0	10.0 5.8	0.6930 0.6930	
	65.6 68.4	1011.0 1003.0	5.4 5.3	0.6930 0.6930	Committee of the commit
	<i>Z</i> Z	= 40.0	NET= 12		
	0.0	OPS= 26 2193.0	ETA= 0.0 162.0	0.6930	
	1.7	2194.0	162.0	0.6930	
•	4•2 6•2	2184.0 2168.0	159.0 154.0	0.6930 · 0.6930	
	8.3 9.2	2147.0 2139.0	147.0 144.0	0.6930 0.6930	
	12.7	2109.0	134.0	0.6930	
	14.9 16.9	2092.0 2080.0	129.0 126.0	0.6930 0.6930	
	# 7 * 7				

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		APPENDIX	A (CONTI.)	
		and the second second	Markin mari in marin in Anna	Distribution of the state of
	R	T	P	F .
NAME I TORONOMO AND	19.6	2075.0	124.0	0.6930
	22.3	2097.0	131.0	0.6930
	24.9	2153.0	146.0	0.6930
	27.2	2254.0	186.0	
	29.4	2532.0	327.0	0.6930
	31.3	2464.0	286.0	0.6930
	33.6	2369.0	236.0	0.6930
	35.6	2287.0	199.0	0.6930
	37.6 39.8	2198.0 2098.0	164.0 131.0	0.6930 0.6930
	42.6	1972.0	97.0	0.6930
	44.8	1869.0	76.0	0.6930
	48.1	1715.0	52.0	0.6930
	48.8	1680.0	46.0	0.6930
	49.0	3300.0	424.0	0.6910
	50.5	3909.0	435.0	0.880.u
	52.5	4705.0	469.0	0.6330
		NOPS= 27	ETA= 10.	0 .
	0.0	2193.0	162.0	0.6930
	1.7	2194.0	162.0	0.6930
	4.2	2184.0	159.0	0.6930
antana masakan da sasa sasa ga jangan masa da ka	6.2	2168.0	154.0	0.6930
the state of the s	8.3	2147.0	147.0	0.6930
	9.2	2139.0	144.0	0.6930
	12.7	2109.0	134.0	0.6930
	14.9	2092.0	129.0	0.6930
	16.9	2080.0	126.0	0.6930
and the second second second second	19.6	2075.0	124.0	0.6930
	22.3	2097.0	131.0	0.6930 0.6930
	24.9	2153.0 2254.0	146.0 186.0	0,6930
	29.4	2532.0	327.0	U.6930
	31.3	2464.0	286.0	0.6930
	33.6	2369.0	236.0	0.6930
	35.6	2287.0	199.0	0.6930
	37.6	2198.0	164.0	0.6930
	39.8	2098.0	131.0	0.6930
	42.6	1972.0	97.0	0.6930
	44.8	1869.0	75.0	0.6930
	48.1	1715.C	52 . 0	0.6930
•	50.0	1640.0	41.0	0.6930
•	50.1	3380.0	406.0	0.6910
	50.8	3702.0	413.0	0.6900
	52.9	4567.0	454.0	0.6510
	53.3	4692.0	450.0	0.6330
	MANAGEMENT OF THE PARTY OF THE	NOPS= 27	ETA= 20.	
	0.0 1.7	2193.0 2194.0	162.0 162.0	0.6930 0.6930
	4.2	2194.0	159.0	0.6930
	6.2	2168.0	154.0	0.6930
	8.3	2147.0	147.0	0.6930
	9.2	2139.0	144.0	0.6930
		arming tratted and Total Co. M. (1994)	naminata Ta Talis To Tanang isan	the state of the s

R T P F 12.7 2109.0 134.0 0.6930 144.9 2052.0 125.0 0.6930 16.9 2080.0 125.0 0.6930 21.6 2080.0 125.0 0.6930 22.3 2057.0 131.0 0.6930 22.3 2057.0 131.0 0.6930 22.4 2153.0 146.0 0.6930 27.2 2254.0 186.0 0.6930 21.1 256.0 0.6930 21.2 252.0 186.0 0.6930 21.3 256.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.4 252.0 186.0 0.6930 21.5 186.0 0.6930 21.6 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 18.6930 21.8 1877.0 977.0 187.0 977.0 187.0 977.					
14.9 2092.0 129.0 0.6930 10.9 2090.0 120.0 0.6930 12.6 2075.0 124.0 0.6930 22.3 2097.0 131.0 0.6930 24.9 2153.0 146.0 0.6930 27.2 2254.0 186.0 0.6930 37.4 2382.0 3277.0 0.6930 31.2 246.0 269.0 0.6930 31.3 246.0 269.0 0.6930 33.4 2265.0 236.0 0.6930 37.6 2198.0 164.0 0.6930 37.6 2198.0 164.0 0.6930 42.16 1972.0 37.0 0.6930 42.16 1972.0 37.0 0.6930 44.1 1715.0 22.9 0.6930 51.3 564.0 34.0 0.6930 52.9 1500.0 28.0 0.6930 52.9 1500.0 28.0 0.6930 53.0 3513.0 358.0 0.6930 53.0 3513.0 358.0 0.6930 54.2 2188.0 162.0 0.6930 55.3 3513.0 358.0 0.6930 51.7 2194.0 162.0 0.6930 51.7 2194.0 162.0 0.6930 52.19 210.0 162.0 0.6930 53.0 213.0 358.0 0.6930 53.0 213.0 358.0 0.6930 53.0 213.0 358.0 0.6930 54.2 2188.0 159.0 0.6930 55.3 36.0 34.0 0.6930 57.2 2188.0 147.0 0.6930 57.2 2188.0 147.0 0.6930 57.3 2198.0 120.0 0.6930 57.5 2198.0 120.0 0.6930 57.5 2198.0 120.0 0.6930 57.5 2254.0 180.0 0.6930 57.5 2255.0 227.0 0.6930 57.5 2258.0 237.0 0.6930 57.5 2258.0 237.0 0.6930 57.5 2258.0 237.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.6930 31.3 2464.0 286.0 0.	Territoria de la composició de la compos	K	T	P	E
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	14.9	2092.0	129.0	0.6930	
	16.9	2080.0	126.0	0.6930	
	19.6	2075.0	124.0	0.6930	
		2097.0	131.0	U.693U	
CONTRACTOR	24.9	2153.0	146.0	0.6930	мен жазана селең қарақында электемен // лизи кенесе ж. 1.1 менеен жазақ қарақ қарақ қарақ қарақ қарақ қарақ жаз
	27.2	2254.0	186.0	0.6930	
· · · · · · · · · · · · · · · · · · ·	29.4	2532.0	327.0	0.6930	
		2464.0	286.0	0.6930	
	33.6	2369.0	236.0	0.6930	
	35.6	2287.0	199.0	0.6930	
	37.6	2198.0	164.0	0.6930	
	39.8	2098.0	131.0	0.6930	
	42.6	1972.0	97.0	0.6930	
		1869.0	76.0	0.6930	Control of the Design Control of the Species
		1715.0	52.0	0.6930	
a sono materiale di successi di conserva d	51.5 54.8	1564.0 1421.0	34.0 23.0	0.6930 0.6930	der adriebensen bestättigt statisticker vilk in der eine eine eine
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	59.1	1249.0	13.0	0.6930	
	61.8	1148.0	9.2	0.6930	
		3847.0	229.2	0.6870	
	63.2	4334.0	223.0	0.6620	
		4461.0	223.0	0.6490	
**************************************	nier meers werken was en bas on ein keers was	OPS= 30	ETA= 40.0		
	0.0	2193.0	162.0	0.6930	· · · · · · · · · · · · · · · · · · ·
	1.7	2194.0	162.0	0.6930	
	1484 ANS. 3.3. / ISC 2006 DOT 1/04/38/35 NOSESSON NOSES		159.0	V.6930	
	6.2	2168.0	154.0	0.6930	
	8.3	2147.0	147.0	0.6930	
	9.2	2139.0	144.0	0.6930	
	12.7	2109.0	134.0	0.6930	트리 그 영화는 사람들 하루레 이 경험
	14.9	2092.0	129.0	0.6930	
	16.9 19.6	2080.0 2075.0	126.U 124.U	0.6930 U.6930	
	22.3	207.0	131.0	0.6930	
	24.9	2153.0	146.0	0.6930	
	27.2	2254.0	186.0	0.6930	
	29.4	2532.0	327.0	0.6930	옷이 그는 그들은 동생들은 다니다.
	31.3	2464.0	280.0	0.6930	
	33.6	2369.0	236.0	0.6930	
	35.6	2287.0	199.0	0.6930	
400 Marie 1997 (1998)	37.6	2198.0	164.0	0.6930	
	39.8	2098.0	131.0	0.6930	
	42.6	1972.0	97.0	0.6930	
	44.8	1869.0	76.0	0.6930	
	48.1	1715.0	52.0	0.6930	
					and the state of t

	R	T	P	e mana 122 sa F	
	51.5	1564.0	34.0	0.6930	
	54.8 59.1	1421.0 1249.0	23•0 13•0	0.6930 0.6930	
	64.7	1055.0 1000.0	6.4 4.4	0.6930 0.6930	g Marika, indisk, silangan samar adalah sejerah propertya kanak angan dan kana
	66.8	4260.0	189.0	0.6680	
	67.9 68.5	4401.0 4399.0	180.0 180.0	0.6530 0.6530	
	Marie Company of the	OPS= 30 2193.0	ETA= 45.0 162.0		
	1.7	2194.0	162.0	0.6930	
	4.2 6.2	2184.0 2168.0	159.0 154.0	0.6930 0.6930	
	8.3 9.2	2147.0 2139.0	147.0 144.0	0.6930 0.6930	
Alle de la companya d	12.7	2109.0	134.0	0.6930 0.6930	ran gustan abasa ng kang salah asa natandaka.
	14.9 16.9	2092.0 2080.0	129.0	0.6930	
	19.6 22.3	2075.0 2097.0	124.0 131.0	0.6930 0.6930	
The state of the s	24.9 27.2	2153.0 2254.0	146.0 185.0	0.6930 0.6930	
1944 sakad di baki sadi dakad ka adda Albacad sak	29.4	2532.0	327.0	0.6930	
	31.3	2464.0 2369.0	286.0 236.0	0.6930 0.6930	
	35.6 37.6	2287.0 2198.0	199.0 164.0	0.6930 0.6930	
a a a superior de la compansión de la comp	39.8	2098.0	131.0	0.6930	
	42.6 44.8	1972.0 1869.0	97.0 76.0	0.6930	
	48.1 51.5	1715.0 1564.0	52.0 34.0	0.6930 0.6930	
	54.8	1421.0	23.0	0.6930	
. A kar, and a pelanest managers (12.2 kg/s/kg/s/kg/s/	59.1 64.7	1249.0 1052.0	13.0 6.4	0.6930 0.6930	
	69.1 73.5	96 7. 0 959 . 0	4.5 4.3	0.6930 0.6930	
	73.6	4237.0	175.0	0.6680	
	73.7 N	4406.0 IOPS= 30	173.0 ETA= 60.0	0.6510)	Televisia Televisia (m. 1904) Televisia (m. 1904)
	0.0	2193.0 2194.0	162.0 162.0	0.6930 0.6930	
	4.2	2184.0	159.0	0.6930	Parkets of the second of the second control of the second control of the second of the second of the second of
	6.2 8.3	2168.0 2147.0	154.U 147.U	0.6930 0.6930	
	9.2 12.7	2139.0 2109.0	144.0 134.0	0.6930 0.6930	
	14.9	2692.0	129.0	. 0.6930	
	16.9 19.6	2080.0 2075.0	125.0 124.0	0.6930 0.6930	
	22.3 24.9	2097.0 2153.0	131.0 146.0	0.6930 0.6930	
paration resident are included and the					

		,	4		A 10
		APPENDIX	A (CONTI.)		A-18
			es anno merco de la la composició de la comp	ene de la companya d	<u>and the state of </u>
	R	Ť	Р	F	
	0.7	2254 0	10/ 0	0 4020	다 보고 있는 사람들이 되었다. 그 사람들은 사람들이 되었다. 그 사람들이 되었다.
	27.2	2254.0 2532.0	186.0 327.0	0.6930 0.6930	
	31.3	2464.0	286.0	0.6930	
	33.6	2369.0	236.0	0.6930	
	35.6	2287.0	199.0	0.6930	iggi, <u>segunda m</u> anggangan manggan kanggan kanggan kanggan manggan manggan manggan manggan manggan manggan menggan Manggan menggan
	37.6	2198.0	164.0	0.6930	
	39.8	2098.0	131.0	0.6930	
	42.6	1972.0	97.0	0.6930	
	44.8	1869.0	76.0	0.6930	
	48.1	1715.0	52.0	0.6930	t de la companya del companya de la companya del companya de la co
	51.5 54.8	1564.0 1421.0	34.0 23.0	0.6930 0.6930	
A. N. Marine St. Const.	59.1	1249.0	. 13.0	0.6930	
		1052.0	0.4	0.6930	
	73.8	958.0	4.4	0.6930	
	76.6	950.0	4.2	0.6930	
4 100 100 100 100 100 100 100 100 100 10	76.7	4257.0	171.0	0.6680	
	76.9	4410.0	169.0	0.6500	•
		NOPS= 29	ETA= 75.0		
	0.0	2193.0	162.2	0.6930	
	1.7	2194.0	162.0	0.6930	
Control of the second s	4.2 6.2	2184.0 2168.0	159.0 154.0	0.6930 0.6930	production of the amplitude to the production of the second section of the second section of the second section of
	8.3	2147.0	147.0	0.6930	
	9.2	2139.0	144.0	0.6930	
	12.7		134.0	0.6930	
	14.9	2092.0	129.0	0.6930	
	16.9	2080.0	126.0	0.6930	ig jakks til deskillarin kolonindis i rijskir brasser gadi tiranset et er er kalikar
	15.6	2075.0	124.0	0.6930	
	22.3	2097.0	131.0	0.6930	
	24.9	2153.0 2254.0	146.0 185.0	0.6930 0.6930	
	27.2 29.4	2532.0	327.0	0.6930	and the second second second second
	31.3	2464.0	286.0	0.6930	Fig. 1. State that we say the first the control of
	33.6	2369.0	236.0	0.6930	
	35.6	2287.0	199.0	0.6930	
	37.6	2198.0	164.0	0.6930	
	39.8	2098.0	131.0	0.6930	
	42.6	1972.0	97.0	0.6930	and the second s
	44.8	1869.0	76.0	0.6930	
	48.1 51.5	1715.0 1564.0	52.0 34.0	0.6930 0.6930	
料 电自变流	54.8	1421.0	23.0	0.6930	
	59.1	1249.0	13.0	0.6930	
	64.7	1052.0	6.4	0.6930	
	69.1	967.0	4.5	0.6930	100
	73.8	958.0	4.4	0.6930	The second of th
*	78.1	1140.0	4.8	0.6930	
		NOPS= 29	ETA= 90.0		
	0.0	2193.0	102.0	0.6930	

2194.0 162.0 0.6930 2184.0 159.0 0.6930

A 224 C	. 240		IXA	 	
11 11 1	1 -	n i i	1 X /	1 . IV	

a mili sakantak paga		Sanahari da Sanahari da kabada da arib	arkiamina dari katalah	er K. D. J. Berger van Sterre van de Britansk van Sterre van de Britansk van de Britansk van de Britansk van d	And Carlotte Comments and the control of the contro
	R	τ ,	P	F	
	6.2	2168.0	154.0	0.6930	
	8.3	2147.0	147.0	0.6930	
	9.2 12.7	2139.0 2109.0	144.0 134.0	0.6930 0.6930	
	14.9	2092.0	129.0	0.6930	
	16.9	2680.0	126.0	0.6930	
	19.6 22.3	2075.0 2097.0	124.0 131.0	0.6930 0.6930	
	24.9	2153.0	146.0	0.6930	
	27.2	2254.0 👑	186.0	0.6930	udosas s
	29.4	2532 • 0 2464 • 0	32 7. 0 286.0	0.6930 0.6930	
	33.6	2369.0	236.0	0.6930	;¥*
	35.6	2287.0	199.0	0.6930	
	37.6	2198.0	104.0	0.6930	
and the second s	39.8 42.6	2098.0 1972.0		0.6930 0.6930	skeris degi is som kilosega. Visins e kertines i gest tip komentaj sem eneksjativa dip
· f	44.8	1869.0	76.0	0.6930	
	48.1	1715.0	52.0	0.6930	
	51.5 54.6	1564.0 1421.0	34.0 23.0	0.6930 0.6930	
	59.1	1249.0	13.0	0.6930	
Librogramming of Romer and Marine and Allinder and Allind	64.7	1052.0	6.4	0.6930	ea market kan
	69.1	967.0	4.5	0.6930	w.
	73.8 78.4	958.0 945.0	4.4 4.1	0.6930 0.6930	
		NUPS= 29	ETA=120.		
	0.0	2193.0	162.0	0.6930	
	1.7	2194.0 2184.0	162.0 159.0	0.6930 0.6930	
	6.2	2168.0	154.0	0.6930	
	8.3	2147.0	147.0	0.6930	
	9.2 12.7	2139.0 2109.0	144.0 134.0	0.6930 0.6930	
	14.9	2092.0	129.0	0.6930	
	16.9	2080.0	126.0	0.6930	
	19.6 22.3	2075.0 2097.0	124.0	0.6930	
			131.0 146.0	0.6930 0.6930	
	24.9 27.2	2153.0 2254.0	191.0 146.0 186.0	0.6930 0.6930	
	24.9 27.2 29.4	2153.0 2254.0 2532.0	146.0 186.0 327.0	0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3	2153.0 2254.0 2532.0 2464.0	146.0 186.0 327.0 286.0	0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4	2153.0 2254.0 2532.0	146.0 186.0 327.0	0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0	146.0 186.0 327.0 286.0 236.0 199.0 164.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6 39.8	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0 2098.0	146.0 186.0 327.0 286.0 236.0 199.0 164.0 131.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6 39.8 42.6	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0 2098.0 1972.0	146.0 186.0 327.0 286.0 236.0 199.0 164.0 131.0 97.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6 39.8	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0 2098.0	146.0 186.0 327.0 286.0 236.0 199.0 164.0 131.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6 39.8 42.6 44.8 48.1 51.5	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0 2098.0 1972.0 1869.0 1715.0 1564.0	146.0 186.0 327.0 286.0 236.0 199.0 164.0 131.0 97.0 76.0 52.0 34.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	
	24.9 27.2 29.4 31.3 33.6 35.6 37.6 39.8 42.6 44.8 48.1	2153.0 2254.0 2532.0 2464.0 2369.0 2287.0 2198.0 2098.0 1972.0 1869.0 1715.0	146.0 185.0 327.0 286.0 236.0 199.0 164.0 131.0 97.0 76.0 52.0	0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930 0.6930	

oder bar strakelik terrikkelik terrikalisi salah s	ed de la compo	legises Crista State	Market and the second of the second s	antinia di none in company, na disadi da mandadhilanda	and a company of the
	R	,	۲	r	
	59.1	1249.0	13.0	- 0.6930	
	64.7	선거 없었다.	6.4	0.6930	
	69.1	967.0 958.0	4.5 4.4	0.6930 0.6930	The state of the s
e to the state of	78.4	945.0	4.1	0.6930	and the state of t
<i>y</i>		NUPS= 29	LTA=180.0		
1	0.0	2193.0	162.0	0.6930	
	1.7 4.2	2194.0 2184.0	162.0 159.0	0.6930 0.6930	
		2168.0	154.0	0.6930	The state of the s
*	8.3	2147.0	147.0	0.6930	
\$	9.2	2139.0	144.0	0.6930	
	12.7	2109.0 2092.0	134.0 129.0	0.6930 0.6930	
	16.9	2080.0	126.0	0.6930	
	19.6			0.6930	<u>a de la companya del companya de la companya de la</u>
·	22.3	2097.0	131.0	0.6930	
	24.9	2153.0	146.0	0.6930 0.6930	
	27.2 29.4	2254.0 2532.0	186.0 327.0	0.6930	
	31.3	2464.0	286.0	0.6930	
	33.6		<u>236.U</u>	0.6930	وماللين والراميدي والرام والمرامي والمرام والمرام والمرام والمرام والمرام والمرام
Company of the State of the Sta	35.6	2287.0	199.0	0.6930	
	37.6 39.8	2198.0 2098.0	164 _* 0 131 _* 0	0.6930 0.6930	
	42.6	1972.0	97.0	0.6930	
	44.8	1869.0	76.0	0.6930	
i de l'accidente l'accidente de la company de la compa	48.1	1715:0	52.40	0.6930	<u> </u>
	51.5	1564.0	34.0	0.6930	the control of the base of the state of
	54.8 59.1	1421.0 1249.0	23.0 13.0	0.6930 0.6930	
	64.7		0.4	0.6930	
	69.1	967.0	4.5	0.6930	
in the same of	73.8	558.0	4.4	0.6930	
	78.4	945.0 Z= 60.0	4.1 NET= 13	0.6930	
		NOPS= 27	ETA= 0.0)	
	0.0	2012.0	107.0	0.6930	
	0.5	2012.0	107.0	0.6930	
	2.3 5.4	2013.0 2020.0	107.0 109.0	0.6930 0.6930	
	6.9	2029.0	111.0	0.6930	
	8.3	2032.0	112.0	0.6930	
	9.8	2034.0	113.0	0.6930	
40	11.9	2031.0	112.0	0.6930	
	12.8 16.5	2029.0 2023.0	111.0 110.0	0.6930 0.6930	A three the the that he was the same the sent the said of the
	18.8	2027.0	111.0	0.6930	
	21.0	2051.0	117.0	0.6930	
	22.9	2115.0	136.0	0.6930	
	25.2	2360.0	232.0	0.6930	
Carlo Ca	27.5 30.2	2304.0 2236.0	207.0 178.0	0.6930 0.6930	Management of the state of the
			and the state of	and the second s	

APPENDIX A (CC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E
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	10-28 100 3 110 110	
	S. A. A. M. M. M. L. T. C.	
	25 35 11 70 20 20 1900	
		S
ALBORO CONTROL TAKAN SON AND S	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	٥
CONTRACTOR	C 100 100 100 100 100 100 100 100 100 10	5
	4.5. 5.77.74. 3.5.575	

30000 37 00 0000 000 000 0000 0000 0000	R	Ţ	Р	F	
					그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그
NAMES AND ASSOCIATION OF THE STATE OF THE ST	32.7	2170.0	154.0	0.6930	
	35.7	2088.0	128.0	0.6930	
	38.5	2011.0	107.0	0.6930	and the second s
and an array of the sales of the sales of the sales of	42.0	W. W. C.	Charles Martin Martin Commerce Control of the Section of the Commerce of the C	0.6930	
	44.9	1821.0	68.0	0.6930	
	45.6	1800.0 2940.0	64.0 379.0	0.6930 0.6930	
**************************************	45.8 47.1	3147.0	381.0	0.6930	
	49.2	3723.U	390.0	0.6900	
	52.3				
	52.5	4644.0	405.0	0.6380	
	4. T = T = T	NOPS= 27	ETA= 10.		
	0.0	2012.0	107.0	0.6930	
	0.5	2012.0	107.0	0.6930	
	2.3	2013.0	107.0	0.6930	
e aliabatate de la companya de la c	5.4	2020.0	109.0	0.6930	
	6.9	2029.0	111.0	0.6930	
	8.3	2032.0	112.0	0.6930	
	9.8	2034.0	113.0	0.6930	
	11.9	2031.0	112.0	0.6930 0.6930	
	12.8 16.5	2029.0 2023.0	111.0 110.0	0.6930	
anditabumanasining (comments)	18.8	2027.0	111.0	0.6930	
	21.0	2051.0	117.0	0.6930	
	22.9	2115.0	136.0	0.6930	三、医院各区之际以下以前。管辖基础。
	25.2	2360.0	232.0	0.6930	
	27.5	2304.0	207.0	0.6930	
	30.2	2236.0	178.0	0.6930	
	32.7	2170.0	154.0	0.6930	- 1、現今にも、計画により、1、1、1、1、1、1、1、1、1、1、1、1、1、1、1、1、1、1、1
	35.7	2088.0	128.0	0.6930	
	38.5	2011.0	107.0	0.6930	
	42.0	1907.0	84.0	0.6930	
	44.9	1821.0	68.0	0.6930	
	46.9 47.0	1764.0 2966.0	59.0 370.0	0.6930 0.6930	
	47.5	3068.0	373.0	0.6930	
	49.6	3563.0	380.0	0.6910	그의 이 집안들이들을 그렇게 밝혔다.
	52.4	4462.0	400.0	0.6610	
	53.3	4643.0	400.0	0.6370	
	47.17	NOPS= 28	ETA= 20.		
	0.0	2012.0	107.0	0.6930	CONTRACTOR OF THE CONTRACTOR O
	0.5	2012.0	107.0	0.6930	그리는 이번 경험 과일에 불어질을 하는데
	2.3	2C13.0	107.0	0.6930	
	5.4	2020.0	109.0	0.6930	
	6.9	2029+0	111.0	0.6930	la production de la company
	6.8	2032.0	112.0	0.6930	
	9.8 11.9	2034.0	113.0 112.0	0.6930 · 0.6930	
	12.8	2031.0 2029.0	111.0	0.6930	
	16.5	2023-0	110.0	0.6930	
	18.8	2027.0	111.0	0.6930	
	21.0	2051.0	117.0	0.6930	
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dia di salah s		APPENUIX A	(GONTI.)		
	Ŕ	T	<i>0.</i>	F F	
	22.9 25.2	2115.0 2360.0	136.0 232.0	0.6930 0.6930	
	27.5 30.2	2304.0 2236.0	207.0 178.0	0.6930 0.6930	
	32.7 35.7	2170.0 2088.0	154.0 128.0	0.6930 0.6930	
	38.5 42.0	2011.0 1907.0	107.0 84.0	0.6930 0.6930	
<u>uniteratura di Particologia di Albara</u>	44.9 48.0 49.9	1621.0 1729.0 1658.0	68.0 54.0 44.0	0.6930 0.6930 0.6930	And the second s
	50.0 50.8	3118.0 3216.0	355.0 353.0	0.6930 0.6930	
	53.3 55.7	3954.0 4603.0	360.0 381.0	0.6870 0.6420	
San	N	4633.0 OPS= 28	379.0 ETA= 30.0		
	0.0 0.5 2.3	2012.0 2012.0 2013.0	107.0 107.0 107.0	0.6930 0.6930 0.6930	
	5.4 5.9	2015*0 2020*0 2029*0	109.0	0.6930 0.6930	
	8.3 9.8	2032.0 2034.0	112.0 113.0	0.6930 0.6930	
	11.9 12.8	2031.0 2029.0	112.0	0.6930 0.6930	
	16.5 18.8	2023.0 2027.0	110.0	0.6930 0.6930	gang di kanggang di kangga Manang di kanggang di kang
	21.0 22.9 25.2	2051.0 2115.0 2360.0	117.0 136.0 232.0	0.6930 0.6930 0.6930	
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	32.7 35.7	2170.0 2088.0	154.0 128.0	0.6930 0.6930	
	38.5 42.0	2011.0 1507.0	107.0 84.0	0.6930 0.6930	
	44.9 48.0 51.4	1821.0 1729.0 1629.0	68.0 54.0 41.0	0.6930 0.6930 0.6930	
	55.7 55.8	1509.0 1508.0	29.0 29.0	0.6930 0.6930	
	55.9 57.4	3268.0 3767.0	309.0 311.0	0.6910 0.6890	
	barran kan kan daran daran kan daran kan daran dar	4596.0 OPS= 29	327.0 ETA= 35.		
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Traped States	8.3	2032.0	112.0	0.6930	

. C. 2 Person and Assistantial	da da o cada	i kalista ka	minima de la compansión d De la compansión de la compansi	lid kilima in a ang kata basa da F	k. Sitah puntu dikencerangan kitabah dia kan kana diken katarita ndarakat bikan kan kina mengengan kenaran seba
	R		P	r.	•
•	9.8	2034.0	113.0	0.6930	
	11.9	2031.0	112.0	0.6930	
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and the second	/16.5//	2023.0	110.0	0.6930	en e
5	18.8	2027.0	111.0	0.6930 0.6930	도마리 그는 것으로 가게 됐다.
	21.0	2051.0 2115.0	117.0 136.0	0.6930	민들은 얼마를 살아 있다.
	25.2	2360.0	232.0	0.6930	
	27.5	2304.0	207.0	0.6930	
en e	30.2	2236.0	173.0	0.6930	<u>initi an ika katang ka</u>
	32.7	2170.0	154.0	0.6930	
	35.7	2088.0	128.0	0.6930	
	38.5 42.0	2011.0 * 1907.0	107.0 84.0	0.6930 0.6930	
	44.9	1621.0	68.0	0.6930	
	48.0		54.0	0.6930	
LIBERT CONTRACTOR PET TREATMENT CONTRACTOR STATEMENT CONTRACTOR CONTRACTOR STATEMENT CONTRACTOR CONTRACTOR STA	51.4	1629.0	41.0	0.6930	
	55.7	1509.0	29.0	0.6930	
	59.0	1410.0	22.0	0.6930	
	59.5 59.6	1399.0 3395.0	21.0 274.0	0.6930 0.6900	
	62.1	4109.0	281.0	0.6790	tana ing kalangan dalam pangan ang kalangan dalam d
	64.1	4560.0	288.0	0.6410	
		NOPS= 30	ETA= 40.	and the second of the second o	
	0.0	2012.0	107.0	0.6930	
	0.5	2012.0	107.0	0.6930	
	2.3	2013.0	107.0 109.0	0.6930 0.6930	
2011 W. (1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814 - 1814	5.4 6.9	2020.0 2029.0	111.0	0.6930	
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	16.5	2023.0 2027.0	110.0	0.6930 0.6930	
	21.0	2051.0	117.0	0.6930	
	22.9	2115.0	136.0	0.6930	
	25.2	2360.0	232.0	0.6930	
	27.5	2304.0	207.0	0.6930	
	30.2	efractivities are viscous commenters and a contractive and a contractive and	<u> 178.0</u>	0.6930	
	32.7 35.7	2170.0 2088.0	154.0 128.0	0.6930 0.6930	
	38.5	2011.0	107.0	0.6930	
	42.0	1907.0	84.0	0.6930	
	44.9	1821.0	68.0	U.6930	
	48.0	1729.0	54.0	0.6930	
	51.4	1629.0	41.0	0.6930	
	55.7	1504.0	29.0	0.6930	
	59.0 64.3	1407.0 1268.0	22.0 14.0	0.6930 0.6930	
	64.5	1260.0	14.0	0.6930	
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	AL ACAD SERVICE CONTROL CONTRO				

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*:	R	T	P	F	
Office and the second s	64.6	3591.0	232.0	0.6890	
	67.1	4258.0	240.0	0.6690	
	68.5	4511.0	242.0	0.6440	
		NORS= 30 /	ETA= 45.	A COUNTY OF STATE OF THE PROPERTY OF THE PROPE	and the second of the second s
	0.0	2012.0	107.0	0.6930	
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	11.9	2031.0	112.0	0.6930	
Į.	12.8	2629.0	111.0	0.6930	
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and the same and t	25.2	2360.0	232.0	0.6930	
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}	30.2	2236.0	178.0	0.6930	
	32.7	2170.0	154.0	0.6930	
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na an a dhe na chine an	38.5	2011.0	107.0	0.6930	
	42.0	1907.0 1821.0	84.0 68.0	0.6930 0.6930	
	48.0	1729.0	54.0	0.6930	
	51.4	1629.0	41.0	0.6930	
	55.7	1504.0	29.0	0.6930	
	59.0	1407.0	22.0	0.6930	
	64.3	1265.0	14.0	0.6930	
	69.7 70.5	1131.0 1117.0	8.6 8.1	0.6930 0.6930	
	70.5	3793.0	3.1 182.1	0.6870	
	72.8	4233.0	187.1	0.6670	
	74.2	4438.0	186.0	0.6480	
ACCOUNTS OF THE PROPERTY OF TH		NOPS= 30	ETA= 60	• 0	The state of the s
	0.0	2012.0	107.0	0.6930	
become an order of the control of th	2.3	2013.0	107.0	0.6930	
	5.4 6.9	2020.0 2029.0	109.0 111.0	0.6930 0.6930	
The second second	8.3	2032.0	111.0	0.6930	
1	9.8	2034.0	113.0	0.6930	
全国人名英国约德 国	11.9	2031.0	112.0	0.6930	
	12.8	2029.0	111.0	0.6930	
1	16.5	2023.0	110.0	0.6930	
	18-8	2027.0	111.0	0.6930 0.6936	
	21.0 22.9	2051.0 2115.0	117.0 136.0	0.6930 0.6930	
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	27.5	2304.0	207.0	0.6930	一种的复数 医骨髓管管脊髓系统
	30.2	2236.0	178.0	0.6930	
	32.7	2170.0	154.0	0.6930	
The state of the s	35.7	2088-0	128.0	0.6930	
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203	25.50	20.2%	V342.7	L. They	32 283	122	23776	0.000	30.5.2.5	4.00	120	100	43.25	1 Z	222	22.37	20,735	1000	3783	12000	3.3293	6 68.75	200	278, TO 16 TO	war is	8 23 KK	5 Sec. 3	10.22	200	CALCO.	93,77635	2.80	2013/00/20
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17	Sec. 35.	20	Sec. 3	32.8	1. 165	19.9%	2000	4. 3.983	1,24	200	S 134	(7), 1	SOM:			: · · · /	183			30E 3	Sec. 17.	V 1630	25 gg,	(4 V 4)	de		253.98	33.79	520	3,70	X	1911	1411
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					er jager al district continue research pare d'Austre accompant à 1950.
Left 17 of 1830/2011 - Co. administration of the 2011 September 1830/2011 of convention of the 2011 September 1830/2011 Septem	R	T	P	F	
	38.5	2011.0	107.0	0.6930	
	42.0	1907.0	84.0	0.6930	
	44.9	1821.0 1729.0	68.0 54.0	0.6930 0.6930	
	51.4	1629.0	41.0	0.6930	i ga pala dhan ag a nin da bha a an da bha an a da dha ga a a 1870 a bha an an saidh an an an air an an an air Can an a
	55.7	1504.0	29.0	0.6930	
	59.0	1407.0	22.0	0.6930	
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	69.7 73.5	1128.0 1044.0	8.5 6.2	0.6930 0.6930	
	73.6	3977.0	167.0	0.6870	
	74.2	4074.0	166.0	0.6760	
A SPECIAL PROPERTY AND	76.9	4401.0	165.0	0.6510	
	0.0	NOPS= 30 2012.0	ETA≃ 75. 107.0	0.6930	
	2.3	2013.0	107.0	0.6930	
	5.4	2020.0	109.0	0.6930	
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- Die Wysikke beginne de Andrea II obe - Berekende sooner beginne de Andrea II ook	8.3	2032.0 2034.0	112.0 113.0	0.6930 0.6930	
	11.9	2031.0	112.0	0.6930	a participate to the participate of the participate
	12.8	2029.0	111.0	0.6930	and the state of t
G. G. D. C. G.	16.5	2023.0	110.0	0.6930	
加加 名字的位为。	18.8	2027.0	111.0	0.6930	
	21.0	2051.0 2115.0	117.3 136.0	0.6930 0.6930	
	25.2	2360.0	232.0	0.6930	
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William And The Control of the Contr	30.2	2236.0	178.0	0.6930	STATE OF THE PARTY OF THE STATE
	32.7 35.7	2170.0	154.0 128.0	0.6930 0.6930	
	38.5	2001.0	107.0	0.6930	
	42.0	1907.0	84.0	0.6930	
e ali mas i sul didustria de Sala de estado de casa.	44.9	1821.0	<u>6</u> 8.0	0.6930	andalisation of the second section of the second section is subsequen
· · · · · · · · · · · · · · · · · · ·	48.0 51.4	1729 _* 0 1629 _* 0	54.0 41.0	0.6930 0.6930	
	55.7	1504.0	29.0	0.6930	
	59.0	1407.0	22.0	0.6930	
	64.3	126540	14.0	0.6930	
<u>, i i santa asperatantin di manada</u>	69.7 75.0	1128.0 1009.0	8.5 5.4	0.6930 0.6930	
	83.3	871.0	3.0	0.6930	
	83.4	4210.0	131.0	0.6670	
	85.7	4350.0	141.0	0.6540	
	· AA	NOPS= 29	ETA= 90.		
	0.0 5.4	2012.0 2020.0	107.0 109.0	0.6930 0.6930	
	6.9	2029.0	111.0	. 0.6930	
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		and the second second		aliinin kalenda araa araa araa araa araa araa araa a	

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		APPENDIX	A (CUNTI.)	ing sa		
	R	T	P	F		for the second s
	18.8	2027.C 2051.0	111.0 117.0	0.6930 0.6930		
	22.9 25.2	2115.0 2360.0	136.0 7232.0	0.6930 0.6930	1. 1888 J. W. W.	
	27.5 30.2	2304.0 2236.0	207.0 178.0	0.6930 0.6930		
	32.7 35.7	2170.0 2088.0	154.0 128.0	0.6930 0.6930	Same and Same to Secure	
	38.5 42.0	2011.0 1907.0	107.0 84.0	0.6930 0.6930	an Mariana di Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupa Kabupatèn Kabupatèn	
	44.9 48.0	1821.0 1729.0	68.0 54.0	0.6930 0.6930		
	51.4 55.7	1629.0 /1504.0	41.0 29.0	0.6930 0.6930		
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	82.0 89.8	875.0 867.0	3.0 2.9	0.6930 0.6930		
	94.9 97.9	858.0 1582.0	2+8 5+8	0.6930 0.6930	1947 1948 - Santa Barrieri, 1948 - Santa Barrieri, 1948 - Santa Barrieri, 1948 - Santa Barrieri, 1948 - Santa Barrieri	
	0.0	NOPS= 30 2012.0	ETA=105. 107.0	0.6930		
	5.4 6.9	2020.0 2029.0	109.0 T11.0	0.6930 0.6930	la de la companya de La companya de la co	
	8.3 // // 9.8 //	2032.0 2034.0	112.0 113.0	0.6930 0.6930		
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	16.5 18.8	2023.0 2027.0	110.0 311.0	0.6930 U.6930		
in a Legin emile i fizik bir 1855 - Legin Brak Brak Brak Brak	21.0 22.9	2051.0 2115.0	117.0 136.0	0.6930 0.6930		
	25.2 27.5	2360.0	232.0 207.0	0.6930 0.6930		
	30.2 32.7 35.7	2236.0 2170.0	178.0 154.0	0.6930 0.6930 0.6930		
	38.5 42.0	2088.0 2011.0 1907.0	128.0 107.0 84.0	0.6930 0.6930	production of the state of the	
	44.9 48.0	1821.0 1729.0	68.0 54.0	0.6930 0.6930		
	51.4 55.7	1629.0	41.0 29.0	0.6930 0.6930	Constitution of the second	
	59.0 ⁸	1407.0 1265.0	22.0 14.0	0.6930 0.6930		
	69.7 75.0	1128.0	8.5 5.4	0.6930		
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Part of the second	94.9	858.0	2.8	0.6930	
	98.4	853.0	2.7	0.6930	English Commission
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	5.4 6.9	2020.0 2029.0	109.0 111.0	0.6930	
	8.3	2032.0	112.0	0.6930 0.6930	
	9.8 11.9	2034.0 2031.0	113.0 112.0	0.6930 0.6930	
and the state of t	/12.8	2031.0 2029.0	;;iii;o;;	0.6930	Control of the state of the sta
	16.5 18.8	2023.0	110.0	0.6930 0.6930	
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a de la companya de	27.5	2304.0	207.0	0.6930	n de la companya del companya de la companya del companya de la co
· 传感为"冷漠"。	30.2	2236.0 2170.0	178.0 154.0	0.6930 0.6930	
	35.7	2088.0	128.0	0.6930	
	38.5 42.0	2011.0 1907.0	107.0 84.0	0.6930 0.6930	
e i go i karana uniya waki waki waki wa	44.9	1821.0	68.0	0.6930	
	48.0 51.4	1729.0 1629.0	54.0 41.0	0.6930	
	55.7	1504.0	29.0	0.6930	
	59.0 64.3	1407.0 1265.0	22.0 14.0	0.6930 0.6930	
. Proces a de Riddon de la Vida de La Vida de Calendario.	69.7	1128.0	8.5	0.6930	
1 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	75.0 82.0	1009.0 875.0	5.4 3.0	0.6930 0.6930	
and the second s	89.8	867.0	2.9	J.6930	
	94.9 98.4	858.0 853.0	2.8 2.7	0.6930 0.6930	
		NOPS= 30	ETA=180.	.0	
	0.0 5.4	2012.0 2020.0	107.0 109.0	0.6930 0.6930	
iorini y valeni sali sali vi di organi sali sali sali sali sali sali sali sal	6.9	2029.0	111.0	0.6930	
	8.3 9.8	2032.0 2034.0	112.0 113.0	0.6930 0.6930	
<u> </u>	11.9	2031.0	112.0	0.6930	
	12.8 16.5	2029.0 2023.0	111.0 110.0	0.6930 0.6930	
	18.8	2027.0	111.0	0.6930	
	21.0	2051.0 2115.0	117.0 136.0	0.6930 0.6930	
	25.2	2360.0	232.0	0.6930	
	27.5 30.2	2304.0	207.0 178.0	0.6930 0.6930	
	32.7	2170.0	154.0	0.6930	
Wester Commen	35.7 38.5	2088.0 2011.0	128.0 107.0	0.6930 0.6930	
and the state of t	42.0	1907.0	84.0	0.6930	
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ii taa liistiin alka kankistana ka	K	T	ing and an addition can P	F		
		,	,	•		
	44.9	1821.0	68.0	0.6930		
	48.0	1729.0	54.0	0.6930		
	51.4	1629.0	41.0	0.6930		
	55.7	1504.0	29.0	0.6930		
	59.0	1407.0	22.0	0.6930		
	64.3	1265.0	14.0	0.6930		
	69.7	1128.0	8.5	0.6930		• 4
	75.0	1009.0	5.4	0.6930		
	82.0	875.0	3.0	0.6930		
	89.8		2.9	0.6930		and the second s
	94.9/	858.0	2.8	0.6930	•	
	98.4	853.0	2.7	0.6930		ration of the second
		Z= 80.0	NET= 13			
		NOPS= 27	ETA= 0.	0		The state of the s
	0.0	1883.0	79.0	0.6930		
	1.0	1883.0	79.0	0.6930		and the second second second
3	5.1	1892.0	81.0	0.6930		
	5.9	1894.0	81.0	0.6930	•	
	7.2	1897.0	82.0	0.6930		
	8.6	1902.0	83.0	0.6930		
	10.7	1915.0	85.0	0.6930		
	12.4	1929.0	88.0	0.6930		
, s	14.0	1941.0	91.0	0.6930		
	15.7	1958.0	94.0	0.6930	•	
	17.8	1997.0	103.0	0.6930		
	18.7	2026.0	111.0	0.6930		
	20.0	2201.0	165.0	0.6930		
	20.7	2291.0	201.0	0.6930		
	21.9	2266.0	190.0	0.6930	ſ	
	25.7	2176.0	156.0	0.6930	5	
	30.3	2062.0	121.0	0.6930	- ,	
	33.4	1998.0	104.0	0.6930		
	37.0	1921.0	86.0	0.6930		
	140.3	1849.0	73.0	0.6930		
	41.7	1820.0	67.0	0.6930		
	41.9	2730.0	319.0	0.6930		
	43.4	2840.0	324.0	0.6930		
	45.7	3125.0	325.0	0.6930		
	48.9	3817.0	329.0	0.6890		
	52.2	4530.0	339.0 338.0	0.6490 0.6440		
	52.5	4570.0 NOPS= 27	ETA= 10.			
	0.0	1883.0	79.0	0.6930		
	1.0	1883.0	79.0	0.6930		
	5.1	1892.0	81.0	0.6930		
	5.9	1894.0	81.0	0.6930		
	7.2	1897.0	82.0	0.6930		
	8.6	1902.0	83.0	0.6930		高级建筑 机流流
	10.7	1915.0	85.0	0.6930		
	12.4	1929.0	88.0	0.6930		
	14.0	1941.0	91.0	0.6930		
	15.7	1958.0	94.0	0.6930		
)	17.8	1997.0	103.0	0.6930		Lastinaulter jeroberer j
,	2100	227180	2000	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		
3					그렇게 많다	

A CONTRACTOR CONTRACTOR	R	is en en antique de la constitue de la constit	Arionalia (Carania) P	ining and a substitution	and a suit was the character of a section of the se
	11	•	•	•	
	18.7	2026.0	111.0	0.6930	
	20.0 20.7		165.0 201.0	0.6930 0.6930	
	21.9		80 P 3 G C WAS SELECTED AS SECURIO SERVICE SER	0.6930	
	25.7	2176.0	156.0	0.6930	
The state of the s	30.3	2062.0 1998.0	121.0 104.0	0.6930 0.6930	
	37.0	1921.0	86.0	0.6930	
	40.3	1849.0	73.0	0.6930	
<u> </u>	.42.9	1793.0	63.0	0.6930	in 1881-1887 ka
	43.0	2760.0 2812.0	317.0 321.0	0.6930 0.6930	
	46.1	3050.0	320.0	0.6930	
	Sec. 4. Sec. 18 Sec. 18 Sec. 18	3681.0	325.0	0.6890	
	/52.3 53.3		335.0 334.0	0.6630 0.6430	
Latinian (India) (1) Language and considerate w	ر و ۾ جري	NOPS= 27	ETA= 20.	With Silver Dr. Control of the Contr	
	0.0	1883.0	79.0	0.6930	
	1.0	1883.0	7 9.0	0.6930 0.6930	
	5.1 5.9	1892.0 1894.0	81.0	0.6930	
	7.2	1897.0	82.0	0.6930	
4.7	8.6	1902.0	83.0	0.6930	
	10.7	1915.0 1929.0	85.0 88.0	0.6930 0.6930	
	14.0		91.0	0.6930	
	15.7	1958.0	94.0	0.6930	
	17.8	1997.0	103.0	0.6930	. 1814 (1915) Santa Carlo (1916) Santa Carlo (1916) Santa Carlo (1916) Santa Santa (1916) Santa Santa (1916) S
	18.7 20.0	2026.0 2201.0	111.0 165.0	0.6930 0.6930	
1 .	20.7	2291.0	201.0	0.6930	
	21.9	88 2 6 8 7 7 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	190.0	0.6930	
	25.7 30.3	2176.0 2062.0	156.0 121.0	0.6930 0.6930	
(2) Lie abet troublinden er Elekarioniste state in Salak 	33.4	1998.0	104.0	0.6930	
	37.0	1921.0	86.0	0.6930	
	40.3	1849.0 1761.0	73.0 58.0	0.6930 0.6930	
	46.3	1718.0	52.0	0.6930	The state of the s
	46.4	2807.0	303.0	0.6930	
47	47.5	2900.0	309.0	0.6930	
	50.3 52.9	3323.0 3972.0	310.0 315.0	0.6920 0.6850	. 5 %
	55.9	4568.0	323.0	0.6430	an and the Rank plants of the state of the state of
		NOPS= 28	ETA= 30		
<u> 1825 - A E. LEGIO DE SA PERENCIA DE LA CARTE DE SA C</u>	0.0 1.0	1883.0 1883.0	79.0 79.0	0.6930 0.6930	
	5.1	1892.0	81.0	0.6930	
: 	5.9	1894.0	81.0	0.6930	
	7.2	1897.0	82.0	0.6930	
	8.6 10.7	1902.0 1915.0	83.0 85.0	0.6930 0.6930	

					er i poste i proposta de la compania del compania del compania de la compania del compania del compania de la compania del
	R	I	Ρ	F	in the second
	12.4	1929.0	88.0	0.6930	, , , , , , , , , , , , , , , , , , ,
	14.0 15.7	1941.0	91.0	0.6930 0.6930	
	17.8	1958.0 1997.0	94.0 103.0	0.6930	
	18.7	2026.0	111.0	0.6930	
	20.0 20.7	2201.0 2291.0	165.0 201.0	0.6930 0.6930	
	21.9	2266.0	190.0	0.6930	
	25.7 30.3	2176.0 2062.0	150.0 121.0	0.6930 0.6930	
ziki ka Azalanda kuman kandan da kanda	33.4	1998.0	104.0	0.6930	un bergan der Berger Berger ber der
	37.0	1921.0	86.0	0.6930	
	40.3 44.4	1849.0 1760.0	73.0 58.0	0.6930 0.6930	
	46.1	1681.0	47.0	0.6930	
in the second second second second second	52.5 52.6	//1587.0 2938.0	36.0 279.0	0.6930 0.6930	and a Make, the Sparch Stroke (Make Self) as a second in the account
	52.7	2950.0	279.0	0.6930	a.*
	54.9	3314.0	287.0	0.6920	
	57.5 50.6	3940.0 4558.0	288.0 298.0	0.6860 0.6420	
a salakaran manakaran kanakaran kanakaran	and the second second	NOPS= 29 /	ETA= 35.	0	
in the second	1.0	1883.0 1883.0	79.0 79.0	0.6930 0.6930	
	5.1	1892.0	81.0	0.6930	And the state of t
	5.9	1894.0	81.0	0.6930	
	7.2 8.6	1897.0 1902.0	82.0 83.0	0.6930 0.6930	The state of the s
	10.7	1915.0	85.0	0.6930	
	12.4	1929.0 1941.0	88.0 91.0	0.6930 0.6930	
	15.7	1958.0	94.0	0.6930	
	17.8	1997.0	103.0	0.6930	
ini da si dahir kabupatèn da kabupatèn	18.7 20.0	2026.0 2201.0	111.0 165.0	0.6930 0.6930	disasan ing panggangan ang panggangan ang panggang panggang
	20.7	2291.0	201.0	0.6930	
	21.9 25.7	2266.0 2 176. 0	190.0 156.0	0.6930 0.6930	
	30.3	2062.0	121.0	0.6930	
	33.4	1998.0	104.0	0.6930	
· · · · · · · · · · · · · · · · · · ·	37.0 40.3	1921.0 1849.0	86.0 73.0	0.6930 0.6930	
•	44.4	1760.0	58.0	0.6930	
	48.1 52.8	1681.0 1581.0'	47.0 36.0	0.6930 0.6930	
	56.6	1499.0	28.0	0.6930	
- no no becomplete cuesto del seus communició del cincipa de commencia del del commencia del commenc	56.7	3035.0	260.0	0.6930	The state of the s
	56.8 59.1	3036.0 3467.0	260.0 266.0	0.6930 0.6910	
	61.9	4134.0	269.0	0.6770	
	64.1	4542.0	275.0	0.6420	
				andria, de la company de l	

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	(CUNTI.) TA= 40.(and a standard have side below the short should be standard the standa

	R	T	þ	F _.	
	0.0	1883.0	79.0	0.6930	
	1.0 5.1	1883.0 (1892.0	79.0 81.0	0.6930 0.6930	a production of the state of th
l Lange le sere in Anthrita partici. La trade in Anthrita in a Medidelica de	5.9	1894.0	81.0	0.6930	i kana katan dalah keromenan bertah dalah keperah dan dalah
	7.2	1897.0	82.0	0.6930	
	8.6 10.7	1902.0 1915.0	83.0 85.0	0.6930 0.6930	
	12.4	1929.0	88.0	0.6930	$m_{eff} = m_{eff} = m_{eff}$
glessych i krasiska karakaka situkska situkska s	14.0	1941.0	91.0	0.6930	
	15.7	1958.0	94.0	0.6930	
	17.8 18.7	1997.0 2026.0	103.0 111.0	0.6930 0.6930	
	20.0	2201.0	165.0	0.6930	
	20.7	2291.0	201.0	0.6930	
	21.9 25.7	/2266.0 2176.0	190.0 150.0	0.6930 0.6930	and the second of the second o
	30.3	2062.0	121.0	0.6930	
	33.4	1998.0	104.0	0.6930	
	37.0	1921.0	86.0	0.6930	
	40.3 44.4	1849.0 1760.0	73.0 58.0	0.6930 0.6930	
	48.1	1681.0	47.0	0.6930	
· 建铁矿 被称《音声	52.8	1581.0	36.0	0.6930	
	56.8	1494.0	28.0	0.6930	
	61.0 61.9	1408.0 1389.0	22.0 21.0	0.6930 0.6930	Albert Constant of the Constan
	62.0	3177.0	236.0	0.6930	and the second s
	63.9	3578.0	239.0	0.6900	
	67.3	4327.0 4520.0	246.0 247.0	0.6640 0.6430	
		DPS= 30	ETA= 45.		
	0.0	1883.0	79.0	0.6930	
skile skaleska kalendaria izbeli	5.1	1892.0 1894.0	81.0	0.6930	nonia (trasportura analesta) dia papa dipada dia dalah dipada dipada dipada
	5.9 7.2	1897.0	81.0 82.0	0.6930 0.6930	
	8.6	1902.0	83.0	0.6930	等等不同學學為自然的自然的意思。
	10.7	1915.0	85.0	0.6930	
	12.4 14.0	1929.0 1941.0	88.0 91.0	0.6930 0.6930	
	15.7	1958.0	94.0	0.6930	
	17.8	1997.0	103.0	0.6930	
	18.7	2026.0	111.0	0.6930	
	20.0 20.7	2201.0 2291.0	165.0 201.0	0.6930 0.6930	
	21.9	2266.0	190.0	0.6930	and the state of the
	25.7	2176.0	156.0	0.6930	
	30.3 33.4	2062.0 1998.0	121.0 104.0	0.6930 0.6930	
	37.0	1921.0	66.0	0.6930	
	40.3	1849.0	73.0	0.6930	
	44.4	1760.0	58.0	0.6930	
					가 그는 때 가는 역사회 교육에게 하루 활성했다면서

	Maria de la companio	and the second s			
A commence of the second secon	R	Ţ	Р	F	
1	60.1	1401 0	47 0	0 (020	
	48.1 752.8	1681.0 1581.0	47.0 36.0	0.6930 0.6930	
	56.8	1494.0	28.0	0.6930	
		1406.0	22.0	0.6930	
CONTRACTOR	65.6	1312.0	16.0	0.6930	
	68.4	1557.0	13.0	0.6930	그는 이 이 경험이 많은 그는 사이를 받다.
1	68.5	3382.0	202.0	0.6920	TEES CONTROL OF THE SECOND OF
	69.9		204.0	0.6890	
	72.5	4215.0	210.0	0.6700	
Sand and a second secon	14.2	4483.0 NUPS= 30	211.0 ETA= 60.	0.6450 .//	ar. Message aller producest, et a research solvenie. En reference stop produce beginn
	0.0	1883.0	79.0	0.6930	Section 1997
	5.1	1892.0	81.0	0.6930	
		1894.0	81.0	0.6930	
	7.2	1897.0	82.0	0.6930	
e isla (h. 90). isaniga (h saturitasia)	8.6	Control National Control Contr	83.U	0.6930	an ann an an t-airean aige an t-airean
A Contract	10.7	1915.0	85.0	0.6930	
	12.4	1929.0	88.0	0.6930	
	14.0	1941.0	91.0	0.6930	
	15.7 17.8	1958.0 1997.0	94.0 103.0	0.6930 0.6930	
	18.7	2026.0	111.0	0.6930	and the state of t
and the second s	20.0	2201.0	165.0	0.6930	
	20.7	2291.0	201.0	0.6930	
	21.9	2266.0	190.0	0.6930	
	25.7	2176.0	156.0	0.6930	
	30.3	2062.0	121.0	0.6930	
and the state of t	33.4	1998.0	104.0	0.6930	an en antaren da esta en arros de ballanta a tambén de la presenta de poblemente de
	37.0	1921.0	86.0	0.6930	
	40.3	1849.0 1760.0	73.0 58.0	0.693 0 0.693 0	
	48.1		47.0	0.6930	
	52.8	1581.0	36.0	0.6930	
	56.8	1494.0	28.0	0.6930	
2000 to 400 to 1000 to 4 and 100 to	61.0	1406.0	22.0	0.6930	
	65.6	1311.0	16.0	0.6930	
	71.2	1203.0	11.0	0.6930	
	71.3	3459.0	187.0	0.6910	
	71.4 73.7	3466.0	187.0	0.6910	And the state of t
The Market Brown of the Bridge St.	76.9	3974.0 4466.0	191.0 196.0	0.6830 0.6450	
	10.5	NOPS= 30	ETA= 75.		
	0.0	1883.0	79.0	0.6930	
	5.9	1894.0	81.0	0.6930	
	7.2	1897.0	82.0	0.6930	
	8.6	1902.0	83.0	0.6930	
	10.7	1915.0	85.0	0.6930	
	12.4	1929.0	88.0	0.6930	
	14.0 15.7	1941.0 1958.0	91.0 94.0	0.6930 0.6930	
	17.8	1997.0	103.0	0.6930	
	18.7	2026.0	111.0	0.6930	
					ne material di basa della con establica della

				CONTRACTOR OF THE STATE OF THE	A-33
		APPENDIX	A (CUNTIS)		
errete de la companya	es decre de la como de	addin derina america de dandania (1851	Maria (Las II Las Shacas)	a partiti de la como d La como de la como dela como de la como de	inean a schooling in moderning the late observed as a state of the same of the school of the observed in a school of the
	R	ì	Р	F	
	20.0	2201.0	165.0	0.6930	
	20.7	72291.0	201.0	0.6930	
	21.9	2266.0	190.0	0.6930	
	25.7	2176.0	156.0	0.6930	
Contractive Contra	30.3	2062.0	121.0	0.6930	
	33.4	1998.0	104.0	0.6930	
	37.0	1921.0	86.0	0.6930	
	40.3	1849.0	73.0	0.6930	
	44.4 48.1	1760.0 1681.0	58.0 47.0	0.6930 0.6930	
igi gyan akaban maka akaban nasi bersak 	52.8	1581.0	36.0	0.6930	i ikidekat gantus kindangga dipangan ing mangantuk ing ing tanggan at tindapan ing manduk.
	56.8	1494.0	28.0	0.6930	
	61.0	1406.0	22.0	0.6930	
	65.6	1310.0	16.0	0.6930	
	71.4	1196.0	11.0	0.6930	
	76.0	1111.0	8.0	0.6930	والمنافع والمرافع والمناوع والمناوع والمناوع والمنافع والمنافع والمنافع والمنافع والمنافع والمناوع والمناوع والمنافع
And the second	80.9	1026.0	6.3	0.6930	
	81.0	3746.0	143.3	0.6870	
eganic horacomonico las aproximas y silvas y monesta	82.1	3951.0	142.0	0.6820	
		4393.0	157.0	0.6510	
		NOPS= 30	ETA= 90. 79.0	ALCOHOL: THE PARTY OF THE PARTY	Secretary Commence of the Comm
and the state of t	5.9	1883.0 1894.0	17.V 0.18	0.6930	liki il 10. s. siki iliki. 1900 silik ili iliki pik kiri ilikun pakabinak iki ilikun iliki silik piki ilikun ik
	8.6	1902.0	83.0	0.6930	医乳色质 医静脉 建金银 医多多氏病
	12.4	1929.0	88.0	0.6930	
	14.0	1941.0	91.0	0.6930	
	15.7	1958.0	94.0	0.6930	
and an appropriate which was become a contra	17.8	1997.0	103.0	0.6930	aliose de rende con estados e administrações de proprieta de la como de la co
	18.7	2026.0	111.0	0.6930	THE POST OF STREET SERVICES AND ASSESSED.
	20.0	2201.0	165.0	0.6930	
	20.7	2291.0	201.0	0.6930	
	21.9 25.7	2266.0 2176.0	190.0 196.0	0.6930 0.6930	
	30.3	2062.0	121.0	0.6930	
	33.4	1998.0	104.0	0.6930	and and an analysis of the first financial control of the control
	37.0	1921.0	86.0	0.6930	
	40.3	1849.0	73.0	0.6930	
	44.4	1760.0	58.0	0.6930	
	48.1	1681.0	47.0	0.6930	
	52.8	1581.0	36.0	0.6930	
	56.8	1494.0	28.0	0.6930	
	61.0 65.6	1405.0 1309.0	22.0	0.6930 0.6930	지기 네 이 그는 것 같아? 얼마를 받는다.
	71.4	1196.0	16.0 11.0	0.6930	
	76.U	1110.0	8.0	0.6930	
	83.4	985.0	4.9	0.6930	
	91.0	870.0	3.0	0.6930	
	98.2	797.0	2.1	0.6930	
	102.0	797.0	2.1	0.6930	
	103.0	4174.0	101.0	0.6700	
	104.6	4333.0	136.0	0.6550	
					rangan nga mangan ng mga katalang mangang ng mga ng mg
			•		

				<u> </u>	A-34
	ŊĘ		A (CUNTI.) ETA=105.	Û	
	R .	T	P DATE	16 F	
ab.	0.0 5.9	1883.0 1894.0	79.0 81.0 83.0	0.6930 0.6930 0.6930	and the second s
	6.6 12.4 14.0	1902.0 1929.0 1941.0	88.0 91.0	0.6930 0.6930	
	15.7 17.8 18.7	1958.0 1997.0 2025.0	94.0 103.0 111.0	0.6930 0.6930 0.6930	
NEW SALES WAS ASSESSED.	20.0 20.7	2201.0 2291.0	165.0 201.0	0.6930 0.6930	And the second s
	21.9 25.7 30.3	2266.0 2176.0 2062.0	190.0 156.0 121.0	0.6930 0.6930 0.6930	
	33.4 37.0	1998.0 1921.0	104.0 86.0	0.6930 0.6930	
	40.3 44.4 48.1	1849.0 1760.0 1681.0	73.0 58.0 47.0	0.6930 0.6930 0.6930	
	52.8 56.8	1581.0 1494.0	36.0 28.0	0.6930 0.6930	
	61.0 65.6 71.4	1405.0 1309.0 1196.0	22.0 16.0 11.0	0.6930 0.6930 0.6930	
	76.0 83.4	1110.0 985.0	8.0 4.9	0.6930 0.6930	
ficts dear significates about analysis and significant and sig	91.0 98.2 .06.7	868.0 797.0 790.0	3.0 2.1 2.0	0.6930 0.6930 0.6930	
	15.3	780.0 775.0	1.9 1.9	0.6930 0.6930	
	0.0 5.9	OPS= 30 1883.0 1894.0	79.0 81.0	0.6930 0.6930	
TO THE CASE OF THE	8.6 12.4 14.0	1902.0 1929.0 1941.0	83.0 88.0 91.0	0.6930 0.6930 0.6930	
	15.7 17.8	1958.0 1997.0	94.0 103.0	0.6930 0.6930	
	18.7 20.0 20.7	2026.0 2201.0 2291.0	111.0 165.0 201.0	0.6930 0.6930 0.6930	
	21.9	2266.0 2176.0	190.0 156.0	0.6930 0.6930	
	30.3 33.4 37.0	2062.0 1998.0 1921.0	121.0 104.0 86.0	0.6930 0.6930 0.6930	
	40.3	1849.0 1760.0	73.0 58.0	0.6930 0.6930	
	48.1 52.8 56.8	1681.0 1581.0 1494.0	47.0 36.0 28.0	0.6930 0.6930 0.6930	
				tanan Bakinga (1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	

C 1970, 25 Total CEC, and SEC 2019 AND	R	T	P		1 Province Additional Conference of the Conferen
	(1 O	1405.0	22.0	0.6930	
	61.0	1309.0	16.0	0.6930	
	71.4	1196.0	11.0	0.6930	
	76.0	1110.0	6.0	0.6930	
A STATE OF THE PROPERTY OF THE	83.4	985.0	4.9	0.6930	
	91.0	868.0	3.0	0.6930	
	98.2	797.0	2.1	0.6930	
	106.7 115.3	790.0 780.0	2.0	0.6930 0.6930	
		775.0	1.9	0.6930	
		NOPS= 30	ETA=180.0	4.0-1017.001.11.001.001.001.001.001.001.001.	Andria de la
	0.0	1883.0	79.0	0.6930	
	5.9	1894.0	81.0	0.6930	
	8.6	1902.0	83.0	0.6930	
	12.4	1929.0	88.0	0.6930	
nas <u>sa a la late</u> (militario) en _en e m montra de la la	14,0	1941.0	91.0	0.6930	and the second second second
	15.7	1958.0 1997.0	94.0 103.0	0.6930	*
	18.7	2026.0	111.0	0.6930	
	20.0	2201.0	165.0	0.6930	
	20.7	2291.0	201.0	0.6930	
8. (24) (2.8) (2.4) (2.4) (2.4) (2.4) (2.4) (2.4) (2.4)	21.9	ments and the second was a second to the first of the real party and the second to the second second to the second	190.0	0.6930	an an state of the state of
	25.7	2176.0	156.0	0.6930	•
	30.3	2062.0	121.0	0.6930	
	33.4	1998.0 1921.0	104.0 86.0	0.6930 0.6930	
	40.3	1849.0	73.0	0.6930	
	44.4	1760.0	58.0	0.6930	
	48.1	1681.0	47.0	0.6930	Marie Control Marie Co. 2017 (4
	52.8	1581.0	36.0	0.6930	
	56.8	1494.0	28.0	0.6930	
	61.0	1405.0	22.0	0.6930	
	65*6 71*4	1309.0 1196.0	15.0 11.0	0.6930 0.6930	
	76.0	1110.0	8.0	0.6930	
	83.4	985.0	4.9	0.6930	, •
	91.0	868.0	3.0	0.6930	
	98.2	797.0	2+1	0.6930	
	106.7	790.0	2.0	0.6930	
	115.3	78C•0 775•0	1.9	- 0.6930 0.6930	أوالماريمة فالسائسة
4	118.4	Z = 120.0	1.9 NET= 13	. O 6 0 9 3 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
		NOPS= 29	ETA= 0.0)	
	0.0	1722.0	53.0	0.6930	100000000000000000000000000000000000000
	0.6	1722.0	.53.0	0.6930	
	3.2	1730.0	54.0	0.6930	daning and
	5.1	1736.C	55.0	0.6930	
	6.2 7.3	1740.C 1748.0	55.0° 56.0	0.6930	
	U.8	1748.0	58.0	0.6930	handar share at the same at
	10.0	1787.0	62.0	0.6930	
	11.3	1869.0	76.0	0.6930	
THE CONTROL OF THE THE PROPERTY OF THE PROPERT	13.1	2062.0	120.0	0.6930	Annual Control of the Park Street Street

				State of the state	
The state of the s	R	T	Р	F	
	14.3	2068.0	122.0	0.6930	그 :
	15.1	2C59.0	120.0	0.6930	
	17.8 22.1	202940	111.0 99.0	0.6930 0.6930	en gelegen in de la grande de la
eneralista en	23.5	1981.0 1971.0	97.0	0.6930	iki jirki madan di diperta ana di dalah kiling perjada kadi filay ing di manasan pangangan dalay ang b
	25.4	1945.0	91.0	0.6930	
	27.9 29.0	1907.0 1889.0	84.0 80.0	0.6930 0.6930	
	30.6	1861.0	75.0	0.6930	
gana na kundhura at kha khina ka kh	31.6	1842.0	71.40	0.6930	
	31.8	2544.0 2553.0	261.0 259.0	0.6930 0.6930	
	34.6	2573.0	255.0	0.6930	
	36.4	2613.0	252.0	0.6930	
	38.1 40.7	2672.0 2826.0	247.0 241.0	0.6930 0.6930	
, kie on die sie sie som spanie bouwoje kateuratenikopte t dan. K	44.0	3185.0	240.0	0.6930	The tribung a december of the first and the second
	48.1	3826.0	237.0	0.6880	
	52.5	4438.0 OPS= 29	242.0 ETA= 10.0	0.6540	
	0.0	1722.0	53.0	0.6930	
i parting gan tanàng makambahasa at	3.2	1730.0	54.0	0.6930	erra de la companya
	5.1 6.2	1736.0 1740.0	55.0 55.0	0.6930 0.6930	
	7.3	1748.0	56.0	0.6930	
	8.8	1760.0	58.0	0.6930	
	10.0 11.3	1787.0 1869.0	62.0 76.0	0.6930 0.6930	and the second seco
(4,00k,gi.s silekkaldasidaisisidkaldaskaldkisadabbis	13.1	2062.0	120.0	0.6930	
	14.3	2068.0	122.0	0.6930	
	15.1 17.8	2059.0 2029.0	120.0 111.0	0.6930 0.6930	
	22.1	1981.0	99.0	0.6930	
and the state of t	23.5	1971:0	97.0	0.6930	Manufacture 2 de la companya de la c
	25.4 27.9	1945.0 190 7. 0	91.0 84.0	0.6930 0.6930	
	29.0	1889.0	80.0	0.6930	
	30.6	1861.0	75.0	0.6930	
	31.6 33.1	1842.0 1818.0	71.0 67.0	0.6930 0.6930	
	33.2	2547.0	256.0	0.6930	
	35.1	2566.0	252.0	0.6930 0.6930	
	36.8 38.6	2601.0 2653.0	249.0 245.0	0.6930	
	41.1	2784.0	239.0	0.6930	
The second	44.3 48.3	3112.0 3710.0	240.0 237.0	0.6930 0.6890	nakobinekaikaikaika (k. 1271a.) olehendeka disami kelala
	52.9	4400.0	241.0	0.6580	A SA
over the a transporting of the section of the secti	53.3	4439.0	241.0	0.6540	
	0.0 0.0	DPS= 30 1722.0	ETA= 20.0 53.0	0 0.6930	
	3.2	1730.0	54.0	0.6930	
of the state of th			era en en en esperatorio de la compania de la comp	enemagan da Antonio (1900), in 1900 (1900), in	namananan maran marin kandan kandan kandan kandan kandan kandan di kandan di kandan di kandan di kandan di kan Kandan kandan kanda

			entral transfer		ro and a first transfer of the property of the contract of the
	R	Ť	P		
		14 Land 1	2 8		
	5.1	1736.0	55.0	0.6930	
	6.2 7.3	1740.0 1748.0	55.0 56.0	0.6930 0.6930	
a Anglija sa	6.8	1760.0	58.0	0.6930	
	10.0	1787.0	62.0	0.6930	
	11.3	1869.0	76.0	0.6930	
	13.1	2062.0	120.0	0.6930	그리고 [[한글라이앤드리스 큐버() 캠프라이
	14.3	7.8603	122.0	0.6930	
	15.1	2059.0	120.0	., 0.6930	and the property of the same
galenie deutsche Market Rück, deut Werterschade	17.8	2029.0	vyTŤŤ*Ď	J. 6930	oda kadilika keringga kadi kadi kadi kadi kadi kadi kadi kad
	22.1	1981.0	99.0	0.6930	
	23.5	1971.0 1945.0	97.0 91.0	0.6930 0.6930	그는 속사를 잃었다. 그 싫어 회사 원
	27.9	1907.0	84.0	0.0930	
	29.0	1889.0	80.0	0.6930	
	30.6	1861.0	75.0	0.6930	
6.7.3.0 cm surficient transmission through constant management frame	31.6	1842.0	71.0	0.6930	
	33.3	1815.0	67.0	0.6930	
THE CANADA SHAPE CAN'T WARRANCE PROTECTION OF THE CONTROL OF THE CANADA SHAPE CONTROL	36.0	1767.0	59.0	0.6930	TO SECURITY WELL AND LOCATION OF THE CONTROL OF THE ACCOUNT OF THE CONTROL OF THE
	37.3	1744.0	56.0	0.6930	
	37.4	2558.0	241.0	0.6930	
and the second s	38.2 39.9	2574.0 2607.0	241.0 237.0	0.6930 0.6930	
	42.3	2701.0	234.0	0.6930	생생님 사람들 보는 사람들이 모르는 그 모든 것이다.
	45.4	2932.0	232.0	0.6930	
	49.1	3419.0	233.0	0.6910	or and the second secon
	52.9	4057.0	231.0	0.6800	
	55.9	4443.0	235.0	0.6530	na ani a kasan a maka sa mana a maka sa maka s
		NOPS= 30	ETA= 30		
	0.0	1722.0	53.0	0.6930	
	5.1 6.2	1736.0 1740.0	55.0 55.0	0.6930 0.6930	
	7.3	1748.0	56.0	0.6930	
	8.8	1750.0	58.0	0.6930	
	10.0	1787.0	62.0	0.6930	
	11.3	1869.0	76.0	0.6930	
	13.1	2062.0	120.0	0.6930	
	14.3	2.068.0	122.0	0.6930	
	15.1	2059.0	120.0	0.6930	
	17.8	2029.0	111.0	0,6930	and a state of the
	22.1	1981.0 1971.0	99.0 97.0	0.6930 0.6930	
	25.4	1945.0	91.0	0.6930	
	27.9	1907.0	84.0	0.6930	
	29.0	1889.0	80.0	0.6930	
	30.6	1861.0	75.0	0.6930	The state of the s
	31.6	1842.0	71.0	0.6930	The state of the s
en e	33.3	1814-0	67.0	0.6930	
	36.0	1765.0	59.0	0.6930	*
	38.7	1721.0 1676.0	52.0 47.0	0.6930 0.6930	
	41.3	TO 10 * A	71.0	U • U 7 3 V	a a company
	A STATE OF THE STATE OF				Mariantana menderikan dikanan menderikan dikan diberah peranan kada ang perangah paga 1

1, 4

APPENDIX/A (GUNTL.)

ALLE EL SAN GALLE PER CALLE SERVICA DE LA RECENTACIÓN DE SERVICA DE CALLE DE CALLE DE CALLE DE CALLE DE CALLE D	R	T	P	F	
	44.7	1619.0	40.0	0.6930	
	44.8	2602.0	217.0	0.6930	Particular and the second
	44.9 47.7	2606.0 2736.0	217.0 220.0	0.6930 0.6930	and the second s
(1) saataliinist säinikkistoja aletta vaikikkin käi kiniseleksissä älikä	51.1	3029.0	220.0	0.6930	tadii 25 til 18 katisti. 200 kitala misti ministrii saisti kata 12 kilosi 18 kilosi kata 18 kilosi 18 kilosi 1 Tari
	54.4 59.2	3504.0	219.0 224.0	0.6910 0.6670	
	59.2 60.6	4273.0 4447.0	224.0	0.6510	
		NOPS= 30	ETA= 35.		
trais es praesantes en esta esta esta esta esta esta esta esta	0.0 5.1	1722.0 1736.0	53.0 55.0	0.6930 U.6930	emiteliaid dherica aige éalt ma ramais bheachtairean ar paol agus dear ar ann a
	6.2	1740.0	55.0	0.6930	
	7.3 8.8	1748.0 1760.0	56.0 58.0	0.6930 0.6930	
	10.0	1787.0	52.0 62.0	0.6930	
(1786) (1786) - Marsay Pala Sana Pandalahan Sana Sana Sana Sana Sana Sana Sana	11.3	0.8931	79.9	0.6930	ka sabada ay a sabadhir sagar ana 14 gu, ana dhir sa sa sa sa
A Shake	13.1	2062.0 2068.0	120.0	0.6930 0.6930	
	15.1	2059.0	120.0	0.6930	
	17.8 22.1	2029.0 1981.0	111.0 99.0	0.6930 0.6930	
	23.5	1971.0	97.0	0.6930	
	25.4	1945.0	91.0 84.0	0.6930	36 3%. 4 36 E
	27.9	1907.0 1889.0	80.0	0.6930 0.6930	
	30.6	1861.0	75.0	0.6930	
	31.6 33.3	1842.0 1814.0	71.0 67.0	0.6930 0.6930	
	36.0	1765.0	59.0	0.6930	
	38.7 41.3	1720.0 1675.0	52.0 46.0	0.6930 0.6930	
	45.0	1612.0	39.0	0.6930	
	49.5	1554.0	33.0	0.6930	
and the second s	49.6 49.7	2646.0 2651.0	20 7. 0 207.0	0.6930 0.6930	
	52.8	2847.0	207.0	0.6930	
•	55.8 60.1	3200.0 3894.0	211.0 211.0	0.6930 0.6860	
	64.1	4448.0	216.0	0.6500	
	0.0	NOPS= 30 1722.0	ETA= 40. 53.0	0 0∙6930	
	6.2	1740.0	55.0	0.6930	n de la companya de La companya de la co
	7.3	1748.0	56.0	0.6930	the property of the second state of the second seco
	8.8 10.0	1760.0 1787.0	58.0 62.0	0.6930 0.6930	
	11.3	1869.0	76.0	0.6930	
· · · · · · · · · · · · · · · · · · ·	13.1	2062.0 2068.0	120.0 122.0	0.6930 0.6930	
	15.1	2059.0	120.0	0.6930	
	17.8 22.1	2029.0 1981.0	111.0 99.0	0.6930 0.6930	
	23.5	1971.0	97.0	0.6930	
go - control of the section of the s					······································

and the second s			<u> Parkanan an an an an an an an</u>		and the second s
	R		P . 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.		
	25.4 27.9	1945.0 1907.0	91.0 84.0	0.6930 0.6930	
	29.0	1889.0	80.0	0.6930	
en en station en	30.6 31.6	1861.0 1842.0	75.0 71.0	0.6930 0.6930	
	33.3 36.0	1814.0 1765.0	67.0 59.0	0.6930 0.6930	
	38.7	1720.0 1674.0	52.0 46.0	0.6930 0.6930	
Commence of the Commence of th		1612.0	39.0	0.6930	and the state of t
	49.8 55.1	1544.0 1472.0	32.0 26.0	0.6930	
	55.2 55.3	1468.0 2713.0	26.0 193.0	0.6930 0.6930	
	58.1	2934.0	197.0	0.6930	
The Annual Company of the Company	61.7 65.6	3419.0 4060.0	200.0 201.0	0.6910 0.6790	
	68.5	4446.0 NOPS= 30	204.0 ETA= 45.	0.6490	
September 1	0.0 6.2	1722.0 1740.0	53.0 55.0	0.6930 0.6930	
ita. Mariak wanasa a Madanda Madala Ma	7.3	1748.0	56.0	0.6930	and the second s
	8.8 10.0	1760.0 1787.0	58.0 62.0	0.6930 0.6930	
	11.3 13.1	1869.0 2062.0	75.0 120.0	0.6930 0.6930	
Liver of the second of the sec	14.3	2068.0	122.0	0.6930 0.6930	
Sant Sala Substation Administration 2th 2th and a said	15.1 17.8	2059.0 2029.0	120.0 111.0	0.6930	
	22.1	1981.0 1971.0	99.0 97.0	0.6930 0.6930	
	25.4 27.9	1945.0 1907.0	91.0 84.0	0.6930 0.6930	
e de la companya de La companya de la co	29.0	1889.0	80.0	0.6930	
	30.6 31.6	1861.0 1842.0	75.0 71.0	0.6930 0.6930	
	33.3 36.0	1814.0 1765.0	. 67.0 59.0	0.6930 0.6930	
	38.7 41.3	1720.0 1675.0	52 . 0 46.0	0.6930 0.6930	
Salatarika (S. S. S	45.0	1612.0	39.0	0.6930	
	49.8 55.1	1544.0 1469.0	32.0 26.0	0.6930 0.6930	
	60.0 62.4	1397.0 1367.0	21.0 19.0	0.6930 0.6930	
	62.5	2821.0	178.0	0.6930	
	64.7 67.9	3041.0 3498.0	182.0 184.0	0.6930 0.6910	
\	74.2	4438.0 NUPS= 30	188.0 ETA= 60.	0.6480 0.	
	0.0 6.2	1722.0 1740.0	53.0 55.0	0.6930 0.6930	

				and the second s	
an isan ang mangkang ang kang ang kang ang kang ang kang ang kang ang kang ang ang kang ang ang ang ang ang an	R	T	P	F	
	7.3	1748.0	56.0	0.6930	
427	8.8	1760.0	58.0	0.6930	
	10.0	1787.0 1869.0	62.0 76.0	0.6930 0.6930	
	13.1	2062.0	120.0	0.6930	redigit saaraa ku bul kan kuu Aadara deelee ku u ta'a ka
	14.3	2068.0	122.0	0.6930	
	15.1 17.8	2059.0	120.0 111.0	0.6930	
	22.1	1981.0	99.0	0.6930	
	23.5	1971.0	97.0	<u>, 0.6930</u>	องเกิดเล้าสามารถสาราสเราสาราสาราสาราสาราสาราสาราสาราสารา
	25.4 27.9	1945.0 1907.0	91.0 84.0	0.6930 0.6930	보고 보고 이 사용을 보고 있었다. 그리고 이 보고 있을까요 그 때문다. 1일 1일 - 1일
	29.0	1889.0	80.0	0.6930	
	30.6	1661.0	75.0	0.6930	
	31.6 33.3	1842.0 1814.0	71.0 67.0	0.6930 0.6930	e protesta de la California de California de California de California de California de California de Californi
i den sagan perangan di dalam da Ny faritr'ora di Sagan dalam dala	36.0	1765.0	59.0	0.6930	<u>inga shallan kaba dha kula kula an kaban kaban kaban kaban kaban kaban kaban kula sa kabula.</u>
中非对对对政务 的原	38.7	1720.0	52.0	0.6930	
	41.3 45.0	1675.0 1612.0	46.0 39.0	0.6930 0.6930	
	49.8	1544.0	32.0	0.6930	
Language State of the Control of the	55.1	1465.0	26.0	0.6930	Mills of the Company
	60.0	1397.0	21.0	0.6930	
	65.8	1323.0 2890.0	17.0 172.0	0.6930 0.6930	
	66.U	2912.0	7172.0	0.6930	
	69.1	3311.0	176.0	0.6920	
the state of the s	76.9	4432.0 NOPS= 30	179.0 ETA= 75.	0.6480 0	
	0.0	1722.0	53.0	0.6930	
	6.2	1740.0	55.0	0.6930	
	8.8 10.0	1760.0 1787.0	58.0 62.0	0.6930 0.6930	
	11.3	1869.0	76.0	0.6930	
AND	13.1	2062.0 .	120.0	0.6930	
	15.1 17.8	2059.0 2029.0	120.0	0.6930	원수관 유명성을 취임하는
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	23.5	1971.0	97.0	0.6930	
n i sa katana kinakatah katana kata	25.4 27.9	1945.0 1907.0	91.0 84.0	0.6930 0.6930	en e
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	30.6	1861.0	75.0	0.6930	
	31.6	1842.0 1814.0	71.0 67.0	0.6930 0.6930	
	36.0	1765.0	59.0	0.6930	
	38.7	1720.0	52.0	0.6930	
	41.3	1675.0	46.0	0.6930	
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	36.6	2707.0	208.0	0.6930	
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*	46.3	3645.0	195.0	0.6890	
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	2.5	1787.0	62.0	0.6930	연간소리 시작하다 소소하다
	3.4	1802.0	65.0 69.0	0.6930 0.6930	
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THE REAL PROPERTY AND A STATE OF THE PROPERTY	8.2	1884.0	80.0	0.6930	
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e e dipercial (de 12 de junto de 12 de	^A , 14.5	1871.0	77.0	0.6930	
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	28.3	2452.0	209.0	0.6930	
	31.8	2514.0	212.0	0.6930	
	36.0	2640.0	207.0	0.6930	
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	43.7	3229.0	195.0	0.6930	
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	0.0	1700.0	50.0	0.6930	
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	3.4	1802.0	65.0	0.6930	
	4.8	1826.0	69.0	0.6930	
A CONTRACTOR OF STREET AND STREET AND STREET	5.7 7.3	1842.0	71.0 76.0	0.6930 0.6930	Linkhaudi Bulun Kupa Linkul () . Link Linkul () . Linku
	7.2 8.2	1867.0 1884.0	80.0	0.6930	
	9.6	1915.0	85.0	0.6930	
	10.0	1947.0	92.0	0.6930	
	11.2 13.2	1925.0 1891.0	87.0 81.0	0.6930 0.6930	

		APPENDIX A I	CONTI.)		A-43
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	R	T	Р	F	
,	4.5	1871.0	77.0	0.6930	
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TO MESSE CONTROL OF A CONTROL OF A SECURIOR AND A			97.0	0.6930	
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	9 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1707.0 1787.0	51.0 62.0	0.6930 0.6930	
a rece : h shidestrue a si ti es straiball alledible ca	College Colleg	1802.0	65.0	0.6930	
		1826.0	69.0	0.6930	
		1842.0	71.0	0.6930	
		1867.0	76.0	0.6930	
Paragraphic Committee		1884.0 1915.0	80.0 85.0	0.6930 0.6930	
a pour est est distribute d'ambie de altre de	Decay and Advanced ventors and according	1947.0	92.0	0.6930	rkaci di Makainistini arkisti di Siddi adilia. Idi adi salah ini di salah salah salah salah s
1	1.2	1925.0	87.0	0.6930	
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	Data talah dari da Baran da B	1780.0	61.0	0.6930	
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		1748.0	56.0 50.0	0.6930	and the state of t
	Control of the Contro	1706.0 1676.0	46.0	0.6930	
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A) L 2 g Bill of the William States of Conference of the States of the	35.0	1641.0	42.0	0.6930	den estama de la lación de la compania de la compa
			189.0	0.6930	
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31 * * ** ** ** ** ** ** ** ** ** ** ** *			L89.0	0.6930	
J to the second of the second	14.1	2673.0	186.0	0.6930	
			180.0	0.6930	·····································
			174.0	0.6890	
			L76.0 ETA= 35.0	0.6580	
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	38•7	1606.0	38.0	0.6930	
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	46.8	1509.0	29.0	0.6930	
	47.0	1505.0	28.0	0.6930	
	47.1	2503.0	169.0	0.6930	
	48.2	2528.0	169.0	0.6930	la kanalah pida keranti kalaman didakan dan kalah salah pila penjalaji kengan penjalah dan kalah baha kan
	50°3 54°4	2595.0 2813.0	167.0 164.0	0.6930 0.6930	
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Anna Cales and Miller from the control of the programment of the street	3.4	1802.0	65.0	0.6930	
	4.8	1826.0	69.0 71.0	0.6930 0.6930	
	5.7 7.2	1842.0 1867.0	76.0	0.6930	
	8.2	1884.0	80.0	0.6930	2 Linnas (von 100 tetrinis kalte läiten set fra frank kalten kille ja kalte läände läändes kalten kalten ja ja T
	9.6	1915.0	85.0	0.6930	y.
- Marchine and Alexandra a	10.0 11.2	1947.0 1925.0	92.0 8 7. 0	0.6930 0.6930	
	13.2	1891.0	81.0	0.6930	
	14.5	1871.0	77.0	0.6930	
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	18.8	1809.0	66.0	0.6930	
- second a trice at the common way with the common against a garden	21.3 23.0	1780.0 1760.0	61.0 53.0	0.6930 0.6930	The state of the s
	24.1	1748.0	56.0	0.6930	
(1. 1. in the Color of States and Color of Sta	27.9	1706.0	50.0	0.6930	aran kang ang ang ang ang ang ang ang ang ang
	34.0 38.8	1648.0 1605.0	43.0 38.0	0.6930 0.6930	A.
	43.4	1551.0	33.0	0.6930	4.1
	46.8	1508.0	29.0	0.6930	A STATE OF THE STA
	52.5	1440.0	24.0	0.6930	
	55.2 55.3	1403.0 2569.0	21.0 153.0	0.6930 0.6930	
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	60.2	2812.0	150.0	0.6930	<i>;</i>
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	74.2	4358.0 NOPS≔ 30	152.0 ETA= 60.	0.6550	
)	0.0	1700.0	50.0	0.6930	in the state of the
	1.2	1707.0	51.0	0.6930	,
	2.5	1787.0	62.0	0.6930	
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	8.2	1884.0	80.0	0.6930	
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A STATE OF THE STA	13.2	1891.0	81.0	0.6930	and the state of t
<i>*</i>					*

was use to be a support some of the definition of the support of t	an and a superior and place proceedings on the superior and a supe	er men enne en		A-48
	APPENDIX A	(CONTI.)		
A Committee of the Comm				
Vi salahir menanki manistrak kelandan in dilamin R	inaka melanda meningan berkada salah T	P	<i>F</i>	al annual de la companya del companya del companya de la companya
. N .	1	٠.٣		
14.5	1871.0	77.0	0.6930	
16.0	1848.0	72.0	0.6930	
18.8	1809.0	66.0	0.6930	
21.3	1780.0	61.0	0.6930	and the second section of the second
23.0	1760.0	58.0	0.6930	· · · · · · · · · · · · · · · · · · ·
26.0 31.2	1728.0 1674.0	53.0 46.0	0.6930 0.6930	
36.1	1632.0	41.0	0.6930	
	1567.0	34.0	0.6930	
	1524.0	30.0	0.6930	
49.0 .	1483.0	27.0	0.6930	<i>*</i>
55.7	1395.0	21.0	0.6930	
58.6	1364.0	19.0	0.6930	
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76.4		148.0	0.6540	
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2.5	1787.0 1802.0	62.0 65.0	0.6930 0.6930	n de santa de la companio de la comp
4.8	1826.0	69.0	0.6930	8
5.7	1842.0	71.0	0.6930	
7.2	1867.0	76.0	0.6930	
8.2	1884.0	80.0	0.6930	
9.6	1915.0	85.0	0.6930	and the control of th
10.0	1947.0 1925.0	92.0 87.0	0.6930 0.6930	,
13.2	1891.0	81.0	0.6930	
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16.0	1848.0	72.0	0.6930	
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21.3	1780.0	61.0	0.6930	
23.0 26.0	1760.0 1728.0	58.0 53.0	0.6930 0.6930	
31.2	1674.0	46.0	0.6930	
36.1	1632.0	41.0	0.6930	
42.1	1567.0	34.0	0.6930	
45.6	1524.0	30.0	0.6930	and the state of the
49.0	1482.0	27.0	0.6930	
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36.1 42.1		41.0 34.0	0.6930 0.6930	, 14 94 1
45.5	1524.0	30.0	0.6930	
49.0	A. 40.00 (1990)	27.0	0.6930	
55.8 63.9	1395.0 1299.0	21.0 15.0	0.6930 0.6930	
77.2	1171.0	10.0	0.6930	
92.4		6.1	0.6930	
92.6 92.7		6.0 100.0	0.6930 0.6930	
96.5	3474.0	102.0	0.6900	
105.0	4361.0 NOPS= 30	145.0 ETA=105.0	0.6540	tadan da ara da kata baha da
0.0		50.0	0.6930	
1.2	1707.0	51.0	0.6930	
2.5 3.4	28 (2007) 100 (1007) 1	62.0 65.0	0.6930 0.6930	
4.8		69.0	0.6930	The first one was profit.
2 • 7		71.0	0.6930	and the state of t
7.2		76.0 80.0	0.6930 0.6930	
9.6		85.0	0.6930	
10.0		92.0	0.6930	
11.2 13.2		87.0 81.0	0.6930 0.6930	ti de company de servicio de la company de c
14.5		77.0	0.6930	
16.0		72.0	0.6930	
18.8 21.3		66.0 61.0	0.6930 0.6930	
27.9	1706.0	50.0	0.6930	
38.8		38.0	0.6930	·····································
43.4 46.8		33.0 29.0	0.6930 0.6930	
52.5	1438.0	24.0	0.6930	
59.1	1355.0	18.0	0.6930	
		and the second second second second second	tion has a single-control of the single-cont	and the state of the

				A=50
	APPENDIX	A (CONTI.)		
R	-	P	F	
	9.		9	셨죠
70.2	1238.0	13.0	0.6930	
83.9	1108.0	7.9	0.6930	
100.0	969.0	4.5	0.6930	
118.0	829.0		0.6930	<u></u>
137.0	698.0	1.2	0.6930	in the second
140.0	682.0	1.2	0.6930	
141.0	3909.0	52.0	0.6850	
	4158.0	91.0	0.6650	
	JPS= 30	ETA=120.0		
244414 12444 1444 1444 1444 1444 1444 1	1700.0	50.0	0.6930	ti a con estrar al la la consequent de l'actività de la consequencia
1.2	1707.0	51.0	0.6930	
2.5	1787.0	62.0	0.6930	
3.4	1802.0	65.0	0.6930	
4.8	1826.0	69.0	0.6930	
5.7	1842.0	71.0	0.6930	
	1867.0	76.0	0.6930	and the state of t
8,2	1884.0	80.0	0.6930	
9.6	1915.0	85.0	0.6930	
10.0	1947.0	92.0 87.0	0.6930 0.6930	
11.2 13.2	1925.0 1891.0	81.0	0.6930	
		WAR TO THE TOTAL TOTAL TO THE T	972 TO 10 TO	
14.5	1871.0	77.0 72.0	0.6930 0.6930	
16.0 18.8	1848.0 1809.0	66.0	0.6930	
21.3	1780.0	61.0	0.6930	
	1706.0	50.0	0.6930	
38.8	1605.0	38.0	0.6930	
43.4	1551.0	33.0	0.6930	
46.8	1508.0	29.0	0.6930	Palan Tanamanna orailaini salahkelingan indulingki ing katas kalambani ink
52.5	1438.0	24.0	0.6930	and the second of the second
59.1	1355.0	18.0	0.6930	三十二岁 人名意西埃克 医性多
70.2	1238.0	13.0	0.6930	Fig.
83.9	1108.0	7.9	0.6930	
100.0	969.0	4.6	0.6930	The state of the s
118.0	829.0	2.4	0.6930	
137.0	698.0	1.2	0.6930	
159.0	619.0	0.8	0.6930	
185.0	604.0	0.7	0.6930	
198.0	594.0	0.7	0.6930	
N N	UPS= 30	ETA=180.0)	
0.00	1700.0	50.0	0.6930	
1.2	1707.0	51.0	0.6930	
· 1 1 - 1 - 2.5	1787.0	62.0	0.6930	
3.4	1802.0	65.0	0.6930	
4.8	1826.0	69.0	0.6930	And the second s
5 .7	1842.0	71.0	0.6930	
7.2	1867.0	76.0	0.6930	
8.2	1884.0	80.0	0.6930	
9.6	1915.0	85.0	0.6930	
10.0	1947.0	92.0	0.6930	
11.2	1925.0	87.0	0.6930	
13.2	1891.0 /	81.0	0.6930	
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97	42	1	40	***	T.					1	67.3	6	r.	***	X.		. 1		THE	*	3
Li.	п	640	 3			Г		x	11.	- 71	1500	и.		1 1	38	: 5	- 1	Ł	2	- 25	3

	on the State of th			· · · · · · · · · · · · · · · · · · ·	1C=A
	tation of the state of the stat	APPENDIX	A (CONTI.)		
and the second s	ZZSLOWE W. W. W. W. W. W.	alaka da	ikakindo , , , ,	A Committee of the Comm	and the state of t
	R	T	Р	F	
, and the second					
	14.5	1871.0	77.0	0.6930	
	16.0	1848.0	72.0	0.6930	
	18.8	1809.0	66.0	0.6930	
	21.3	1780.0	61.0	0.6930	
	27.9	1706.0	50.0	0.6930	
	38.8	1605.0	38.0	0.6930	그 그 그 그 사람들이 되는 그들의 것은 그리고 있다.
	43.4	1551.0	33.0	0.6930	그 그는 그 가게 하시네 중 성격이다.
	46.8	1508.0	29.0	0.6930	- commence and the second seco
	52.5	1438.0	24.0	0.6930	
port of the second	59.1	1355.0	18.0	0.6930	
gara pi kalamata di Katamata di Katamat	70.2	1238.0	13.0	0.6930	
	83.9	1108.0	7.9	0.6930	
	100.0	969.0	4.6	0.6930	
		829.0		0.6930	
	118.0		2.4	130.50	
	137.0	698.0	1.2	0.6930	And the second s
n de la companya de	159.0	619.0	0.8	0.6930	and the second comments of the second control of the second secon
1841 3000	185.0	604.0	0.7	0.6930	
	198.0	594.0	0.7	0.6930	
		Z= 200.0	NET= 13	*.	
		NOPS= 30	ETA= 0.0		
	0.0	2240.0	180.0	0.6930	
	1.2	2214.0	170.0	0.6930	To part of the product of the control of the contro
	1.8.	2177.0	157.0	0.6930	
	3.0	2115.0	136.0	0.6930	
	4.0	2059.0	120.0	0.6930	그 그 그 그 그 가장 그렇게 되었다. 그래?
	4.5	2015.0	108.0	0.6930	
	4.6	2718.0	376.0	0.6930	
	4.7	2719.0	377.0	0.6930	100
The control of the co	5.4	2685.0	355.0	0.6930	
마음하다 그 말리 아이트	5.9	2653.0	335.0	0.6930	
	6.3	2653.0	336.0	0.6930	
	6.8	2616.0	313.0	0.6930	114414
	7.4	2589.0	297.0	0.6930	
	8.3	2556.0	279.0	0.6930	
li litariji likuriki kun karanti i karanti kun karanti karanti karanti karanti karanti karanti karanti karanti V	10.2	2506.0.	254.0	0.6930	
	11.5	2482.0	242.0	0.6930	
	13.2	2455.0	229.0	0.6930	
	14.6	2444.0	224.0	0.6930	
	15.5	2455.0	226.0	0.6930	
		2442.0	220.0	0.6930	
	16.5 18.3	2428.0	211.0	and the second s	
				0.6930	
- 医性性衰弱性质点点症	19.4	2421.0	205.0	0.6930	
a Polit Brook and a service of the s	22.2	2415.0	195.0	0.6930	
	25.8	2431.0	185.0	0.6930	
	28.4	2466.0	181.0	0.6930	
· <u> </u>	32.0	2559.0	175.0	0.6930	
	38.0	2854.0	171.0	0.6930	
	43.1	3335.0	175.0	0.6920	
	48.4	3931.0	174.0	0.6840	
	52.5	4293.0	175.0	0.6620	was the same of the
		NOPS= 30	ETA= 10.0		
	0.0	2240.0	180.0	0.6930	
	1.2	2214.0	170.0	0.6930	
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R T P F 1.8 2177.0 157.0 0.6930 3.0 2115.0 136.0 0.6930 4.0 2C59.0 120.0 0.6930 5.0 2009.0 106.0 0.6930 5.8 1963.0 95.0 0.6930 6.6 1921.0 86.0 0.6930 7.0 1921.0 86.0 0.6930 7.1 2606.0 304.0 0.6930 8.9 2519.0 257.0 0.6930 9.6 2501.0 148.0 0.6930 10.7 2479.0 238.0 0.6930 12.0 2458.0 228.0 0.6930 13.7 2436.0 218.0 0.6930 15.9 2443.0 219.0 0.6930 16.9 2433.0 214.0 0.6930 16.9 2433.0 219.0 0.6930 21.3 2407.0 195.0 0.6930 22.3 2407.0 195.0 0.6930 23.5 2490.0 175.0 0.6930 27.7 2479.0 238.0 0.6930 30.5 2490.0 175.0 0.6930 30.5 2490.0 186.0 0.6930 27.7 2437.0 195.0 0.6930 27.7 2437.0 195.0 0.6930 27.7 2437.0 195.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 27.7 2437.0 179.0 0.6930 30.5 2490.0 175.0 0.6930 40.6 3006.0 171.0 0.6930 40.6 3006.0 171.0 0.6930 51.0 4090.0 171.0 0.6930 51.0 4090.0 171.0 0.6930 51.0 172.0 0.6930 51.0 172.0 0.6620 NUPSE 30 ETAE 20.0 0.0 2240.0 180.0 0.6930 1.2 2214.0 170.0 0.6930			HITLION A			
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	29.8	2423.0	166.0	0.6930	ga sa sa
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Application of the second	12.1	1749.0	56.0	0.6930	
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ř	16.2	1685.0	48.0	0.6930	
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	22.8	1626.0	40.0	0.6930	
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•	26.6	2348.0	161.0	0.6930	
	29.8	2362.0	159.0	0.6930	
	32.2	2379.0	157.0	0.6930	
	33.9	2402.0	156.0	0.6930	
Andrewski andrawski status	38.5	2499.0	155.0	0.6930	
	43.0 48.4	2693.0 3075.0	156.0 154.0	0.6930	
•	51.7	3399.0	153.0	0.6910	
	55.2	3788.0	152.0	0.6870	
	60.6	4282.0	153.0	0.6610	
	the state of the second	NOPS= 30	ETA= 35.0		<u> </u>
1.	0.0	2240.0	180.0	0.6930	
	1.2	2214.0	170.0	0.6930 0.6930	
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Ì	7.1	1919.0	86.0	0.6930	
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		APPENDIX /	(CONTIAL)		
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ilia antika kang paga balay na manada.		and a second of the second	likang daman <u>a</u> masa balik stabilik	in the state of th	mana an iku ak dan da kabila kila da ka ki ki kila da kila da kila da ki
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	26.2	1589.0	37.0	0.6930	
	29.8	1556.0	33.0	0.6930	
	31.7	1550.0	33.0	0.6930	
	31-8	2331.0	149.0	0.6930	
No.	31.9	2340.0	149.0	0.6930	
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	37.4	2396.0	148.0	0.6930	property and the second
	42.5	2520.0	149.0	0.6930	and the second of the second
	46.8	2709.0	150.0	0.6930	
	50.8	2994.0	148.0	0.6930	
and the first of the forest of the first of	53.9	3290.0	146.0	0.6930	ga yan da kata kata kata kata kata kata kata k
	59.4	3875.0	144.0	0.6850	
	64.1	4278.0	145.0	0.6610	
		OPS= 30	ETA= 40.0		
	0.0	2240.0	180.0	0.6930	
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*	5.0	2009.0	106.0	0.6930	
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	6.6	1921.0	86.0	0.6930	
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	7.8	1972.0	77.0	0.6930	
* * * * * * * * * * * * * * * * * * *	8.6	1840.0	71.0	0.6930	erandaringan karangan karangan karangan karangan kan karangan karangan karangan karangan karangan karangan kar Karangan karangan ka
	9.7	1802.0	65.0	0.6930	
}	10.6	1779.0	61.0	0.6930	
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Allen and the self-self-self-self-self-self-self-self-	16.2	1685.0	48.0	0.6930	of an administration of the Company
	18.0	1665.0	45.0	0.6930	4
9. 1	22.8	1626.0	40.0	0.6930	
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ale de la companya d	37.8 37.9	2344.0	138.0	0.6930	
S.	38.3	2349.0	138.0	0.6930	
ļ	46.7	2525.0	143.0	0.6930	
	54.3	2929.0	141.0	0.6930	
	57.2	3195.0	138.0	0.6930	
	60.3	3498.0	137.0	0.6900	
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-	67.1	4164.0	136.0	0.6690	
	68.5	4275.0	135.0	0.6600	2 2
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	1.2	2214.0	170.0	30.6930	Constitution in the analysis of the analysis of the angle

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	5.0	2009.0	106.0	0.6930	
and the second	5.8	1963.0	95.0	0.6930	and a second control of the second control o
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	12.1	1749.0	56.0	0.6930	
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Trace of the stranger trace is the second state of the second state of the second state of the second state of	29.9	1550.0	33.0	0.6930	
At Transition	34.9	1502.0	29.0	0.6930	3
Transit Market	38.6	1472.0	26.0	0.6930	
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ง.ค.ปม.ค.ป.ค.ส.เพศประสมเด็จได้เกิดสำนักของสมเด็จได้เกิดสำนัก	46.8 47.9	2409.0	131.0	0.6930	A nariasa, akker ningan ibi sahalah ini asamat dipungan bes
	54.3	2600.0	134.0	0.6930	
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	100000000000000000000000000000000000000	3151.0	130.0	.0.6930	
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11 mai 14. mai 14. mai 14. mai 16. mai	74.2	4273.0 JPS= 30	126.0 ETA= 60.0	0.6590	Landina de la califación de la compansión
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F. A. Carlotte and A. Carlotte	1.2	2214.0	170.0	0.6930	
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المناف الالالمنافقين والمنافقين والمنافق والمناف	9.7	1802.0	65.0	0.6930	
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	13.8	1720.0 1685.0	52.0 48.0	0.6930 0.6930	
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ta. Cen tala 14.0 M. Charles (Charles Control	24.2	1607.0	38.0	0.6930	nn e se sensen menemetrik kristian semekarak pangan diginak kristian di pangan kristian diginak digina
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	36.2 41.2	1490.0 1450.0	28.0 25.0	0.6930 0.6930	
	11.04		2.00	V. U. J. J.	
	and the second second	arada an anarada astrofici.	i dan kalendar or militar kalendar (j. 1832).	a dan Linni, milian kin li bilan kan dan dikelik ji k	enciamentalista meneralista del principio del del como de establica del

COTES OF SHIP TO THE SAME SHIP OF THE STOPP SHIP TO THE STOPP SHIP SHIP SHIP SHIP SHIP SHIP SHIP SH	andromen (1914), rud randalak raksiste etak ar isi	ente entre	a portugui na projeti por projeti por a projeti na projeti na projeti na projeti na projeti na projeti na proj		A-56
		APPENDIX A	(CONTIA)		
in the appropriate continuous and an artist and a super-	E D	kilalinin ora kariban korist kilalinin isaa. T	D	an a	a District a Marie and Land British Self of the State and Albert And And Alber
	K	.1	r	* /	•
	48.7	1391.0	21.0	0.6930	**************************************
	50.5	1385.0	20.0	0.6930	
	50.6	2404.0	129.0	0.6930	
an or a factorist harbed historist that the state of the same of	51.2	2420.0	129.0	0.6930	and the second of the second s
	56.6	2594.0	130.0	0.6930	
ì	63.4	3011.0	127.0 123.0	0.6930	
and the control of the second	68.8 76.9	3534.0 4276.0	123.0	0.6900 0.6590	
		IDPS= 30	ETA= 75.0		
	0.0	2240.0	180.0	0.6930	
D.C. 2011 LEWIS CON A BARRACINA A BARRACINA TO THE ANTICAL PROPERTY OF THE STATE OF	1.2	2214.0	170.0	0.6930	76. (M) SARA (A R. 244 SA) SA IMPERATA IN COMPANIAN SA PROMINING THAN SAMELINE SAMELINE SAMELINE AND AND SAMEL THE SAMELINE SAMELIN
a,	1.8	2177.0	157.0	0.6930	
Express particles, survival proproduction and the control of the c	4.0	2059.0	120.0	0.6930	TO THE RESIDENCE OF THE PROPERTY OF THE PROPER
M. Maria	5.0	72009.0	106.0	0.6930	and the second s
	5.8	1963.0 1921.0	95.0 86.0	0.6930 0.6930	
sieren er ein er eine er ein er eine eine	7.1	1919.0	86.0	0.6930	kirikakakan di aktualisi di aktualisi kirikatak
	7.8	1872.0	77.0	0.6930	
	8.6	1840.0	71.0	0.6930	
	9.7	1802.0	65.0	0.6930	
	10.6	1779.0	61.0	0.6930	
e lan e les la come est est année la se année la se en se la come est en la come en la come est en la come est	12.1	1749.0	56.0	0.6930	er vanska statu da den kana Sera kan mili debanda 100 mili deba
	13.8	1720.0	52.0	0.6930	
	16.2 18.0	1685.0 1665.0	48.0 45.0	0.6930 0.6930	in the state of th
ing a sector de servicio de la company de la	22.6	1626.0	40.0	0.6930	
	24.2	1607.0	38.0	0.6930	
	28.1	1568.0	34.0	0.6930	
\$ 7 % actors to the definite in research months and a state out to receive the second second and a second s	32.8	1521.0	30.0	0.6930	·····································
	36.2	1490.0	28.0	0.6930	
	41.2	1450.0	25.0	0.6930	ernen som en statistiske statistiske statistiske statistiske som en et statistiske statister og en en en en en
	48.7	1390.0	21.0	0.6930 0.6930	
and the second second second	60.6 62.7	1299.0 1284.0	15.0 15.0	0.6930	
La laist, 1927 (La Authra ancioles (La Astronaul La Astro	62.8	2491.0	117.0	0.6930	liddiniski inkalimbili 1300 milioniki kuntiliski enin 1511 i 251 milioni
	62.9	2497.0	116.0	0.6930	
	70.1	2867.0	115.0	0.6930	en e
		3387.0	111.0	0.6910	
	85.7	4285.0	122.0	0.6580	
A CONTRACTOR OF THE PROPERTY O		IOPS= 30	ETA= 90.0		alestes alibertiskus tilletar stormariska i samtet (1771) pre-
	0.0 1.2	2240.0 2214.0	180.0 170.0	0.6930 0.6930	
	1.8	2177.0	157.0	0.6930	$\frac{1}{2} \left(\frac{1}{2} + \frac{1}{2} \right) = \frac{1}{2} \left(\frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right) = \frac{1}{2} \left(\frac{1}{2} + \frac{1}{$
9.5	4.0	2059.0	120.0	70.6930	
	5.0	2009.0	106.0	0.6930	
	5.8	1963.0	95.0	0.6930	And a section with the section of th
}	6.6	1921.0	86.0	0.6930	Strandon and Annual Control of the Strandon and Ann
	7.1	1919.0	86.0	0.6930	
octorial (Salar Mandella) and salar sa A	7.8 8.6	1872.0 1840.0	77.0 71.0	0.6930 0.6930	
	9.7	1802.0	65.0	0.6930	
		1779.0	61.0	0.6930	
for the said of the said the said said said said said said said said				and the second	and the section and the substitution of the su

Production and All republic Control of the Control	R	T.	P	Description of the control of the co
	12.1	1749.0	56.0	0.6930
	SPACE SALL A COUNTY OF A PRINCIPLE OF A SALAR	1720.0	52.0 ///	0.6930
and the second second second		1685.0	48.0	0.6930
man mengelakan kan di dibilah di		1665.0 1626.0	45.0 40.0	0.6930
•		1586.0	36.0	0.6930
<i>t</i>		1550-0	33.0	0.6930
	\$13.28 A A X A A A X B B \$25 B A B A B A B A B A B A B A B A B A B	1501.0	29.0	0.6930
		1471.0	26.0	0.6930
artin interestation in the analysis in the second	45.3 51.8	1416.0 1374.0	22.0 20.0	0.6930 0.6930
		1312.0	16.0	0.6930
	67.5	1239.0	13.0	0.6930
	15 de maria de 18	1081.0	7.1	0.6930
	86.3	1074.0	6.9 89.0	0.6930 0.6930
and a tropical consequences of the all	86.4 90.1	2714.0 2960.0	91.0	0.6930
	105.0	4308.0	128.0	0.6570
	NO	PS= 30	ETA=105.0	
	CONTROL OF THE CONTRO	2240.0	180.0	0.6930
	PROPERTY AND A STATE OF THE PARTY OF THE PAR	2214.0 2177.0	170.0 157.0	0.6930 0.6930
. vi i ne sport spirit iz se kar shinka kili kilika shinka shinka	4.0	2059.0	120.0	0.6930
	5.0	2009.0	106.0	0.6930
	5.8	1963.0	95.0	0.6930
	6.6 7.1	1921.0 1919.0	86.0 86.0	0.6930 0.6930
	7.8	1872.0	77.0	0.6930
galais i a lightabh is iol alleadh an 1921 an deall airt. I	8.6	1840.0	71.0	0.6930
<i>i</i>	9.7	1802.0	65.0	0.6930
	10.6 12.1	1779.0 1749.0	61.0 56.0	0.6930 0.6930
	13.8	1720.0	52.0	0.6930
	16.2	1685.0	48.0	0.6930
	18.0	1665.0	45.0	0.6930
	22.8 28.1	1626.0 1568.0	40.0 34.0	0.6930 0.6930
		1521.0	30.0	0.6930
	41.2	1449.0	25.0	0.6930
	48.8	1390.0	21.0	0.6930
	60.7 65.0	1298.0 1261.0	15.0 14.0	0.6930
	79.6	1130.0	8.5	0.6930 0.6930
	93.1	1027.0	5.8	0.6930
	131.0	793.0	2.0	0.6930
	135.0 136.0	768.0 3353.0	1.8 51.0	0.6930
	140.0	3669.0	53.0	0.6930 0.6850
	148.0	4279.0	120.0	0.6580
		IPS= 30	ETA=120.0	
	0.0 1.2	2240.0 2214.0	180.0 170.0	0.6930 0.6930
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R	,1	P	F	r	*:
1.8	2177.0	157.0	0.6930		
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	1963.0	95.0	0.6930	A COLOR OF THE PROPERTY OF THE	alanging an ear document to the h
6.6 7.1	1921.0 1919.0	86.0 86.0	0.6930 0.6930		
7.8	1872.0	77.0	0.6930		
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9.7	1802.0	65.0	0.6930	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
10.6	1779.0	61.0	0.6930	CASE A STATE OF THE STATE OF TH	
12.1	1749.0	56.0	0.6930	0.6930	*
13.8	1720.0	52.0	0.6930		
16.2	1685.0	48.0	0.6930		nosporantentaria ya se it novat tanan por vi zapan kanan kanan kanan kanan
18.0	1665.0	45.0	0.6930		
22.8	1626.0	40.0	0.6930		
29.9	1550.0 1471.0	33.0 26.0	0.6930		and the artists of the second and others.
38.7 51.8	1374.0	20.0	0.6930		•
63.3	1276.0	14.0	0.6930		
75.7	1165.0	9.7	0.6930		
85.3	1080.0	7.1	0.6930		
102.0	966.0	4.5	0.6930		
121.0	847.0	2.7	0.6930	0.6930	WHITE THE STATE STATE OF THE PERSON SHARES AND STATE OF THE PE
143.0	720.0	1.4	0.6930		•
166.0	624.0	0.8	0.6930		. Ordina projekovija, projek kondronski sovik kinasoliki orom kondronak iz sa
193.0	568.0	0.6	0.6930	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	
220.0	554.0	0.5	0.6930 0.6930	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
234.0	542.0 NOPS= 30	0.5 ETA=180.		U. DYSU	
0.0	2240.0	180.0	0.6930	0.6930	
1.2	2214.0	170.0	0.6930		
1.8	2177.0	157.0	0.6930		
4.0	2059.0	120.0	0.6930	0.6930	
5.0	2009.0	106.0	0.6930	0.6930	
5.8	1963.0	95.0	0.6930		
6.6	1921.0	86.0	0.6930		9
7.1	1919.0	86.0	0.6930		
7.8	1872.0	77.0	0.6930 0.6930		
8.6 9.7	1840.0 1802.0	71.0 65.0	0.6930		
10.6	1779.0	61.0	0.6930		
12.1	1749.0	56.0	0.6930		
13.8	1720.0	52.0	0.6930		
16.2	1685.0	48.0	0.6930		
18.0	1665.0	45.0	0.6930	 2010 100 100 100 100 100 100 100 100 100	
22.8	1626.0	40.0	0.6930		ing and a second se
29.9	1550.0	33.0	0.6930		
38.7	1471.0	26.0	0.6930		
51.8	1374.0	20.0	0.6930		New York and other profit to the profit of t
63.3 76.7	1276.0	14.0 9.7	0.6930 0.6930		
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and the state of t	in a the second contract of the second contra	Miking Baranga Languaga	and the second s	and the second and the second and the second se	and and an included the second

e aryana no a na cipan indra aragén interpretar, o promposarios paga pagantago, que que paga em a se con combi	lingualing and an agriculture of the most of the configuration of the	er og og gang men skripping og skripper og grenne år i en en søpper en systemærene er prøse	A-59
어려운 그림 아름은 경우 중심하는 경우	APPENDIX	A (CONTI.)	
i karamatan kila kerinda dalam kerinda kerinda kerinda kerinda kerinda kerinda kerinda kerinda kerinda kerinda R	deliketedid delimb mellem kiril di si kiril silip siddhimis T	Albert of most of moderate of the	a marining service source and a marine and a marine service service service service service service service ser E
	•		•
85.3	1080.0	7.1	0.6930
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166.0	624.0	0.8	0.6930
193.0 220.0	568.0 554.0	0.6	0.6930
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	Z= 300.0	NET= 13	
	NOPS= 19	ETA= 0.0	
	2666.0	194.0	0.6930
29.0	2666.0	194.0	0.6930
29.3	2664.0	188.0	0.6930
29.6	2660.0	182.0	0.6930
√/////////30.43	// 2672.0	175.0	0.6930
and the comment had been seen to	2690.0	171.0	0.6930 die seine der der der der der der der der der de
31.3	2694.0	168.0	0.6930
32.0	2716.0	164.0	0.6930
32.9 34.8	2747.0 2836.0	160.0 155.0	0.6930 0.6930
36.8	2971.0	155.0	0.6930
38.0	3C57.0	152.0	0.6930
39.0	3123.0	151.0	0.6930
40.5	3248.0	149.0	0.6920
42.1	3370.0	147.0	0.6910
44.4	3560.0	144.0	0.6900
46.6	3760.0	144.0	0.6870
49.0	3967.0	143.0	0.6810
52.5	4200.0	143.0	0.6670
2.2	NOPS= 21	ETA= 10.0	
0.0	2666.0	194.0	0.6930
20.8 28.1	2703.0 2615.0	231.0 189.0	0.6930 0.6930
28.4	2608.0	182.0	0.6930
28.9	2613.0	178.0	0.6930
29.7	2629.0	172.0	0.6930
30.4	2643.0	168.0	0.6930
30.8	2648.0	165.0	0.6930
31.5	2668.0	161.0	0.6930
32.5	2697.0	157.0	0.6930
34.4	2773.0	152.0	0.6930
36.4	2898.0	152.0	0.6930
37.8	2985.0	149.0	0.6930
38.7	3048.0	148.0	0.6930
40.2	3158.0	145.0	0.6930
41.7	3278.0 3458.0	143.0 141.0	0.6920 0.6910
46.2	3653.0	140.0	0.6880
48.5	3860.0	139.0	0.6850
53.2	4182.0	139.0	0.6680
53.3	4192.0	139.0	0.6670
and the second s	NOPS= 30	ETA= 20.0	사람들은 그들이 그는 그는 이 그는 이 그는 그림을 하는 것 같은 그를 가게 되었다. 그는 사람들이 되었다면 하는 것이 되었다면 하는 것 같아. 그를 하는 것 같아 그는 것이다.
0.0	2666.0	194.0	0.6930
20.1	2544.0	230.0	0.6930

Secret and Secret Selection States and Secretaria Selection to the second secretarial sec	R	T	P	ting to the second and the control of the second second to the second second second second second second second F
	21.6	2550.0	224.0	0.6930
	22.8	2546.0	215.0	0.6930
	24.4	2567.0	212.0	0.6930
	25.0	2578.0	211.0	0.6930
Control of the Contro	25.3	2568.0	203.0	0.6930
	25.7	2567.0	200.0	0.6930
or the strong continuous signs and start to the start of	25.9	2530.0	185.0	0.6930
	26.3	2521.0	179.0	0.6930
	26.4	2512.0	175.0	0.6930
s getein ein einschrift till im Schalt till in John und bestände ka	26.9 27.4	2508.0 2509.0	169.0 165.0	0.6930 0.6930
	28.5	2520.0	160.0	0.6930
	29.3	2535.0	151.0	0.6930
	29.7	2540.0	155.0	0.6930
	30.6	2560.0	152.0	0.6930
	31.6	2585.0	149.0	0.6930
	33.5	2641.0	144.0	0.6930
	35.7	2744.0	144.0	0.6930
	37.1	2809.0	142.0	0.6930
	38.0	2856.0	140.0	0.6930
	39.5 41.1	2942.0 3050.0	137.0 135.0	0.6930 0.6930
	43 . 1	3203.0	133.0	0.6930
	45.4	3375.0	131.0	0.6910
	47.7	2558.0	130.0	0.6890
	51.8	3917.0	129.0	0.6840
	55.1	4124.0	129.0	0.6710
	55.9	4174.0	228.0	0.6670
ŀ		IOPS= 30	ETA= 30.	
	0.0	2666.0	194.0	0.6930
	13.2 14.7	2469.0 2450.0	204.0 195.0	0.6930 0.6930
	16.3	2438.0	189.0	0.6930
	18.0	2431.0	183.0	0.6930
A second a retraction of the solution of the s	19.8	2438.0	182.0	0.6930
	21.6	2442.0	178.0	0.6930
•	23.6	2465.0	179.0	0.6930
	24.6	2463.0	174.0	0.6930
	25.0	2456.0	169.0	0.6930
	25.9	2419.0	153.0	0.6930
***************************************	27.3	2404.0	143.0	0.6930 0.6930
	28.4 29.3	2410.0 2418.0	139.0 137.0	0.6930
	30.7	2435.0	133.0	0.6930
	31.8	2453.0	132.0	0.6930
	33.7	2495.0	129.0	0.6930
	35.9	2577.0	131.0	0.6930
Signal Control of the	37.2	2617.0	129.0	0.6930
	38.1	1649.0	128.0	0.6930
	39.5	2707.0	126.0	0.6930
	40.9	2772.0	124.0	0.6930
and the second s	ing in the second second second	Literaturi de Santonia estado esta desta esta desta esta de continuado de continuado de continuado de continuad	enistra anticologia de la compansión de la	and the state of t

	and the state of t	propert encarys o lents a viva vacing carrier or regent 19	A-61	
	APPENDIX A	(CONTI.)		
- 100 per 40 commentativa de casa e della casa della della R	maka menengan salah dan kembanan kembanan kembanan kembanan beranan beranan beranan beranan beranan beranan be T	P	F	1800 - Palas S. Missaul I., Alex S. Herrich and Son Kindeline and Adal San State
·•	•/	,	•	
43.0	2885.0	123.0	0.6930	
45.0 T		121.0	0.6930	
		소리 그 나는 사람들이 가지 않는 사람들은 얼마를 되었다.		4.6
47.1	3158.0	119.0	0.6930	
50.9	3443.0	117.0	0.6910	inglik ferminde eine man net magnetik minglik bestellten
53.8	3676.0	116.0	0.6880	
55.8	3844.0	116.0	0.6850	
59.5	4.093.0	116.0	0.6720	
60.6	4157.0	115.0	0.6670	
N	OPS= 30	ETA= 35.0	the contraction of the section of the	
0.0	2666.0	194.0	0.6930	Marijana kadisa sa kadisa ka
8.4	2475.0	189.0	0.6930	
9.6	2443.0	181.0	0.6930	
12.4	2403.0	172.0	0.6930	
14.0	2392.0	168.0	0.6930	
ī7.i	2384.0	163.0	0.6930	
20.6	2390.0	161.0	0.6930	
(4.4 4 • 4 • 4 • 4 • 4 • 4 • 4 • 4 • 4 •	2414.0	160.0	0.6930	
25.5	2415.0	156.0	0.6930	
<i>y</i>			0.6930	
26.2	2400.0	149.0		
26-3	2382.0	143.0	0.6930	
, 26.8	2369.0	138.0	0.6930	
27.5	2354.0	132.0	0.6930	ing a paragraph and a large and a second of the control of the con
29.3	2357.0	126.0	0.6930	•
30.6	2366.0	124.0	0.6930	
32.7	2390.0	121.0	0.6930	
34.5	2423.0	119.0	0.6930	
36.7	2491.0	122.0	0.6930	
38.0	2526.0	120.0	0.6930	
40.3	2599.0	118.0	0.6930	environment and an environment of the property
. 41.7	2650.0	117.0	0.6930	
43.7	2738.0	115.0	0.6930	
45.6	2839.0	114.0	0.6930	
47.6	2962.0	114.0	0.6930	
51.1	3210.0	112.0	0.6930	
53 . 8	3405.0	110.0	0.6910	interior de la companya de la comp
55.6	3544.0	110.0	0.6890	
59.0	3819.0	109.0	0.6850	
62.9	4084.0	109.0	0.6720	
64.1	4152.0	109.0	0.6670	
		44 CONTRACTOR OF THE PROPERTY	0.0010	
	OPS= 30.	ETA= 40.0		ية مينوني ليدمين بالكناب والأنظال ليست
0.0	2666.0	194.0	0.6930	
4.5	1275.0	14.0	0.6930	
5.6	1293.0	15.0	0.6930	What program is the first own and a second s
6.9	1309.0	16.0	0.6930	
8.2	1323.0	17.0	0.6930	
9.6	1335.0	17.0	0.6930	
10.3	2349.0	120.0	0.6930	And the state of t
11.4	2337.0	125.0	0.6930	
12.5	2328.0	128.0	0.6930	
13.7	2327.0	132.0	0.6930	
15.0	2319.0	133.0	0.6930	
17.8	2321.0	137.0	0.6930	
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	20.9	2333.0	140.0	0.6930	
	24.4	2358.0	142.0,	0.6930	
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	28.0	2347.0	131.0	0.6930	•
,	28.7	2316.0	121.0	0.6930	
3.	29.6	2305.0	116.0	0.6930	
	31.8	2308.0	111.0	0.6930	
	33.2	2318.0	110.0	0.6930	A Sala Sala
page of the page of the time of the second o	36.1	2354.0	108.0	0.6930	er annen gegretagen an en die geste gelekt aben hat it. Einde and besche an ist an en en en en
Marie Control	39.5	2435.0	109.0	0.6930	
	41.7	2492.0	108.0	0.6930	
	45.0	2602.0	106.0	0.6930	
	48.7	2764.0	105.0	0.6930	
	54.4	3132.0	105.0	0.6930	
alantinina a amangana ang talah 19 kandari 1	59.1	3479.0	103.0 102.0	0.6900 0.6860	transceria de la comencia de la compania de la comp
1	62.4 68.5	3749.0 4150.0	102.0	0.6670	
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	11.2"	1343.0	18.0	0.6930	
	12.7	1352.0	18.0	0.6930	
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	17.9	1375.0	20.0	0.6930	
	19.8	1381.0	20.0	0.6930	
	21.8	1387.0	20.0	0.6930	
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	27.5	2312.0	125.0	0.6930	
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	68.9	3811.0	96.0	0.6850	
	74.2	4150.0	95.0	0.6660	
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APPENDIX A (CONTI.)		7
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5.7 1285.0 15.0 0.6930 7.0 1302.0 16.0 0.6930 8.3 1318.0 16.0 0.6930 9.7 1331.0 17.0 0.6930 11.2 1343.0 18.0 0.6930 12.7 1352.0 18.0 0.6930 14.4 1359.0 19.0 0.6930	1				
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9.7 1331.0 17.0 0.6930 11.2 1343.0 18.0 0.6930 12.7 1352.0 18.0 0.6930 14.4 1359.0 19.0 0.6930			V 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	 A. J. C. St. Ville Co. No. 9 (1988) 405 (1988) 105. 	
12.7 1352.0 18.0 0.6930 14.4 1359.0 19.0 0.6930		9.7			0.6930
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		AND THE RESERVE AND ADDRESS OF THE PARTY OF		19.0	0.6930
18.0 1374.0 20.0 0.6930		L8.V/	1374.0	20•0	
19.9 1379.0 20.0 0.6930					
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41.3 2193.0 83.0 0.6930	The second of th	The second secon			THE CONTRACT OF THE PROPERTY O
		None de la constante de la cons	anno de la companya d	enter de la companya	

7	and the state of t	The second of th	e Constant de l'agrecia de la constant de la consta	en e	A-64
		APPENDIX A	(CCNTI.)		
talanda saka saka saka saka kata da ka da ka da ka	Ser Samer of the Service of Albahamaka and Albahamaka	المماملة والمتحدل وواقت والمسافقة	ala dise di 🚉 - dale si didipandika badana	ikantina anda maka maka maka maka maka maka maka ma	a de la companya de l
.	K		P	۲	
3	42.5	2197.0	82.0	0.6930	
	45.1	2215.0	81.0	0.6930	
一个一点 我们,你只要只要这个,我们们,我们不知道,我们就会的情况,我们更好更有知识的最后,我们不	47.9	2257.0	83.0	0.6930	
	52.8	2322.0	82.0	0.6930	
A COMPLEX CONTROLLER AND	60.8	2537.0	81.0	0.6930	adisi di kutu tahungan persamakan kanan digan di pengangan pengan pengangan di pengan dan pengangan pengangan Pengan
,	71.6	3148.0	84.0	0.6930	
*	79.9	3789.0	86.0	0.6850	
	85.7	4164.0	92.0	0.6650	
	OS TRUEBA DE DAMESTA DE LA C	JPS= 30	ETA= 90.0		
and the second of the state behalf the contraction of the second	0.0	2666.0	194.0	0.6930	andras establicas de la companya de
	4.6	1266.0	14.0	0.6930	
•	5.7	1285.0	15.0	0.6930	
	7.0 8.3	1302.0	16.0 16.0	0.6930 0.6930	
	9.7	1331.0	17.0	0.6930	
	11.2	1343.0	18.0	0.6930	
and a survey of the state of the second of t	12.7	1352.0	18.0	0.6930	aarakeelee ah dhaadhaalka ka k
1	14.4	1359.0	19.0	0.6930	
	16.1	1367.0	19.0	0.6930	
Anna Antonia de Caractería	18.0	1374.0	20.0	0.6930	
	19.9	1379.0	20.0	0.6930	
	21.9	1384.0	20.0	0.6930	
provided all was seen and the seen as the see all actions are seen as the seen and the seen are seen as a seen	26.2	1388.0	20.0	0.6930	
	30.8	1385.0	20.0	0.6930	
	33.9	1381.0	20.0	0.6930	
	36.1	1334.0	17.0	0.6930	
	39.3	1265.0	14.0	0.6930	
,	42.1 45.5	1239.0	13.0 11.0	0.6930 0.6930	nami den kanan da
	50.8	1211.0	11.0	0.6930	
	57.8	1153.0	9.3	0.6930	
	62.9	1124.0	8.4	0.6930	
	69.5	1091.0	7.4	0.6930	
	71.0	2300.0	66.0	0.6930	
ti direkt silm. V diner Karlesskerille E tillikettil flækt Efterik Extensionalistiken.	83.4	2726.0	69.0	0.6930	illando filonomo, o en la compaña de la
	89.6	3117.0	70.0	0.6930	
• • • • • • • • • • • • • • • • • • • •	95.5	3542.0	71.0	0.6880	
	L00.0	3896.0	71.0	0.6810	
	L05.0	4193.0	99.0	0.6630	
and the second second second second	Charles Lab. As No. 1. 1935 Charles Street Contraction of the	OPS= 30	ETA=105.0		
	0.0	2666.0	194.0	0.6930	
	4.6	1266.0	14.0 15.0	0.6930 0.6930	•
	5.7 7.0	1285.0 1302.0	15.0	0.6930	
	8.3	1318.0	16.0	0.6930	
	9.7	1331.0	17.0	0.6930	
and the state of the same of t	11.2	1343.0	18.0	0.6930	alderstation in the second attributes and a light and a design and data at the left and taking a recognition of
	12.7	1352.0	18.0	0.6930	
	14.4	1359.0	19.0	0.6930	
	16.1	1367.0	19.0	0.6930	
	18.0	1374.0	20.0	0.6930	
and the second s	19.9	1379.0	20.0	0.6930	iani na dimenganka ing katala kanada kanadangan di dalah na tampan da 1867 kan mang Lington mang menjang

the second of the second control of the second of the seco	in produced in a constant was properties. T	P	F	der bede seit heit einte der Abdulle ist der Batter der der der der Abdulle in der St. der der Abdulle in der Batter der
			~	
21.9	1384.0	20.0	0.6930	
24.1	1386.0	20.0	0.6930	
28.5 33.3	1387.0 1386.0	20.0 20.0	0.6930 0.6930	Control of the second of the s
South and the second states of the second se	1305.0	16.0	0.6930	i disa kanan katina diri dasilasi delek di Espanishing del Krahassaning di
40.9	1250.0	13.0	0.6930	·
45.5	1211.0	11.0	0.6930	
50.8	1197.0	11.0	0.6930	
62.9	1124.0	8.4	0.6930	
75.0	1067.0	6.8	0.6930	Double state in the frequency of the second state of the first term of the second
93.6	987.0	4.9	0.6930	
103.0	950.0	4.2	0.6930	
112.0	912.0	3.6	0.6930	TO MATERIAL STORES STORES STORES SOURCE STORES STORES AND STORES AND STORES STORES SOURCE AND STORES AND STORE
118.0	884.0	3.1	0.6930	
127.0 128.0	839.0 2925.0	2.6 48.0	0.6930 0.6930	
136.0	3427.0	48.0	0.6900	tisaan di madi salah di mada salah di bilan di b
148.0	4221.0	105.0	0.6610	
1	NDPS= 30	ETA=120.		
0.0	2666.0	194.0	0.6930	
4.6	1266.0	14.0	0.6930	
5.7	1285.0	15.0	0.6930	Same and the same of the same
7.0	1302.0	16.0	0.6930	
8.3	1318.0	16.0	0.6930	
9.7	1331.0	17.0	0.6930	
11.2	1343.0	18.0	0.6930	
12.7 14.4	1352.0 1359.0	18.0 19.0	0.6930 0.6930	The second secon
16.1	1367.0	19.0	0.6930	is a Mariante Americki in a colonial and a describe a little de la compactica de la colonial de la colonial de
18.0	1374.0	20.0	0.6930	
26.2	1388.0	20.0	0.6930	
30.8	1385.0	20.0	0.6930	
37.4	1293.0	15.0	0.6930	
44.1	1222.0	12.0	0.6930	
52.6	1185.0	10.0	0.6930	•
62.9	1124.0	8.4	0.6930	
74.8	1067.0	6.8	0.6930	
81.9 93.6	1034.0 987.0	6.0 4.9	0.6930 0.6930	
112.0	912.0	3.6	0.6930	
121.0	867.0	2.9	0.6930	Land of the state
133.0	813.0	2.3	0.6930	
146.0	750.0	1.6	0.6930	
171.0	664.0	1.0	0.6930	
201.0	589.0	0.6	0.6930	
236.0	527.0	0.4	0.6930	
278.0	473.0	0.3	0.6930	to the second of
282.0	4167.0	93.0	0.6640	
287.0	4230.0 NUPS= 30	107.0 ETA=180.	0.6610	
0.0	2666.0	ETA=180.	0.6930	
4.6	1266.0	14.0	0.6930	
y . C. ca a Can manadala sahaidan K. A. Lahi Manadala B. Baha saha aban baha sahaila sahaila a Communishi dalam Y			tudinadatina aina nasana indasisina sultina	utioneedii ottiliisi saa keisse valkisiiski õitkiilikiistististisi. Sii siisiki

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APP	1-11	1 1	хΩ	 	IN I	- 1	.]

a trial Marian Maria Maria di Sala and Maria Sala and Ala and A	R	ndimina sering	P	i da inne de a la caledada de la cal	ana iran anata tersah karasti babba (darika sai da nankiran dasika) baban khisto di nalindiki barastiki karast
	5.7	1285.0	15.0	0.6930	
3.92	7.0	1302.0	16.0	0.6930	
	8.3	1318.0	16.0	0.6930	And the second s
alaba din disebut di Jakana ana mangana da	9.7	1331.0	17.0	0.6930	Local and calculate the control of
	11.2	1343.0	18.0	0.6930	
	12.7	1352.0	18.0	0.6930	\mathcal{L}_{\bullet}
	14.4	1359.0	19.0	0.6930	
	16.1	1367.0	19.0	0.6930	
	18.0	1374.0	20.0	(0 ⋅ 6930)	
a de la companya de	19.9	1379.0	20.0	0.6930	nad died. Die de Lee ee dange van de delegelijk de gemachtelijkel de afdelijs of med de dige gemeen in
	21.9	1384.0	20.0	0.6930	
	26.2	1388.0	20.0	0.6930	
	30.8	1385.0	20.0	0.6930	
	37.4	1293.0	15.0	0.6930	
	44.1	1222.0	12.0	- 0.6930	
	52.6	1185.0	10.0	0.6930	Laci propriation and markets (Appending Section 2.8 has been decided
	62.9	1124.0	8.4	0.6930	
	74.8	1067.0	6.8	0.6930	•
	81.9	1034.0	6.0	0.6930	·
	93.6	987.0	4.9	0.6930	
	112.0	912.0	3.6	0.6930	
ng ang ang ang pag-pagnapan ang pagnapan ang pagnapan ang pagnapan ang pagnapan ang pagnapan ang pagnapan ang	121.0	867.0	2.9	0.6930	
	133.0	813.0	2.3	0.6930	
	146.0	750.0	1.6	0.6930	
	171.0	664.0	1.0	0.6930	
	201.0	589.0	0.6	0.6930	
	236.0	527.0	0.4	0.6930	
pa dada daga da daga ka da na sabah dada daga daga daga daga da daga daga	338.0	527.0	0.4	0.6930	i antinida e antiki manga atauki kataka atau atau

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